## INSTRUCTION MANUAL

## Type 1157-B Scaler ( 500 MHz ) A

## GENERALRADIO

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## WARRANTY

We warrant that each new instrument manufactured and sold by us is free from defects in material and workmanship and that, properly used, it will perform in full accordance with applicable specifications for a period of two years after original shipment. Any instrument or component that is found within the two-year period not to meet these standards after examination by our factory, District Office, or authorized repair agency personnel will be repaired or, at our option, replaced without charge, except for tubes or batteries that have given normal service.

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# Condensed Operating Instructions 

## CAUTION

Be sure the line-voltage switch on the rear of the instrument is properly set for the available power.
a. Turn SENSITIVITY control to the left stop.
b. Connect power plug to a source of power at the correct voltage, using the power cord supplied.
c. Bring the signal of frequency to be measured to the INPUT connector. Max level: 7 V rms.
d. Connect the 10/100 OUT jack to a suitable counter,
such as the GR 1192.
e. Set the MULTIPLY... BY switch to the desired ratio. The pilot light should glow.
f. Turn the SENSITIVITY control cw , as required, to obtain indication in the green sector of the INPUT LEVEL meter. The scaler is now in operation.

## Specifications

## INPUT

Frequency: 1 to 500 MHz .
Minimum Amplitude: 0.3 V pk-pk ( 0.1 V rms ) on most sensitive setting of attenuator.
Maximum Signal: 7 V rms ( 1 W ).
Impedance: AC-coupled, $50 \Omega$.
Attenuator (sensitivity control): Panel switch of $\times 1, \times 2, \times 5$ or $\times 10$ attenuation.
Meter: Green sector indicates adequate signal level for easy adjustment of sensitivity control.
Connector: GR874* locking connector; can be moved to rear panel.
OUTPUTS
Switched Output: DC-coupled positive pulse, >1 V behind $50 \Omega$.
Repetition rate is input frequency divided by 10 or 100 depending on setting of panel switch. Duty ratio is $60 \%$ for $1 / 10$ output, $40 \%$ for $1 / 100$ output.

Sync Output: Positive pulse, $>1 \mathrm{~V}$ behind $50 \Omega$. Repetition rate is input frequency divided by 100 . Duty ratio, $60 \%$. Connectors: BNC; can be moved to rear panel.

## GENERAL

Power Required: 100 to 125 or 200 to 250 V, 14 W.
Accessories Supplied: Power cord; patch cord to 1192 counter. Mounting: Convertible-Bench cabinet.
Dimensions (width $\times$ height $\times$ depth): Bench, $81 / 2 \times 37 / 8 \times 14 \mathrm{in}$. $(220 \times 99 \times 355 \mathrm{~mm})$; rack, $19 \times 31 / 2 \times 123 / 4 \mathrm{in}$. ( $485 \times 89 \times 325 \mathrm{~mm}$ ). Net Weight: Bench $7 \mathrm{lb}(3.2 \mathrm{~kg})$; rack $9.6 \mathrm{lb}(4.1 \mathrm{~kg})$.
Shipping Weight: Bench $9.3 \mathrm{lb}(4.2 \mathrm{~kg})$; rack $13 \mathrm{lb}(5.9 \mathrm{~kg})$.

| Catalog <br> Number | $1157-\mathrm{B}$ Scaler $(500 \mathrm{MHz})$ |
| :---: | :---: |
| $1157-9700$ <br> $1157-9701$ | Bench Model <br> Rack Model |

See General Radio Experimenter, July-August 1969.


Refer to 1192 Instruction Manual for information about the counter.

## Introduction-Section 1

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### 1.1 PURPOSE.

The General Radio 1157-B Scaler extends the upper-frequency limit of any frequency-measuring instrument by a factor of 100 , to a maximum of 500 MHz , by direct-counting techniques.

The scaler can be combined with the GR 1191 or 1192 counters or with the GR 1159 Recipromatic Counter, to measure frequencies up to 500 MHz .

The 1157-B can be used with other frequency counters, oscilloscope synchronizing circuits, analog frequency meters, or in other applications requiring 100-to-1 or 10-to-1 frequency division.

### 1.2 DESCRIPTION.

The scaler is a completely self-contained direct-counting frequency divider that can divide input frequencies from 1 to 500 MHz by factors of 10 and 100 .

The input circuitry consists of a GR874® locking input connector, a four-position attenuator, an input level meter, and a cascode input amplifier that provides better than $100-\mathrm{mV}$ rms sensitivity and also isolates the input from noise generated by the switching circuits. The input level meter aids in proper setting of attenuator or signal-source level. The input amplifier is followed by a scale-of-two divider circuit, triggered by its own pulse generator. Ihis circuit uses tunnel diodes to ensure proper high-frequency operation. Following the scale-of-two divider are a scale-of-five and a scale-of-ten divider, in cascade.

The main output - 10:1/100:1 OUT - comes from the appropriate divider, as determined by the MULTIPLY COUNTER READING BY switch. The final divider also provides the 100:1 SYNC OUT. Both output jacks are BNC.

Input and output connectors may be mounted separately on either front or rear panel. The location has no effect on operating characteristics of the instrument.

### 1.3 CONTROLS, INDICATORS, AND CONNECTORS.

Table 1-1 lists and describes the 1157-B Scaler controls, indicators, and connectors, illustrated by Figure 1-1.

### 1.4 ACCESSORIES SUPPLIED.

The scaler is supplied with a $6-\mathrm{in}$. patch cord, $\mathrm{P} / \mathrm{N}$ 0776-2000 (to connect the 1192 Counter) and a $7-\mathrm{ft}$., 3 -wire power cord, P/N 4200-9622. The rack-mounting version of the scaler includes also a rack adaptor set, P/N 0480-9722.

### 1.5 ACCESSORIES AVAILABLE.

General Radio instruments and accessories that are most frequently used with the scaler are listed in Tables 1-2, 1-3, and 2-2. Refer to the GR catalog for a complete listing of other appropriate accessories, such as attenuators, elbows, meters, etc. The rack adaptor set, GR cat no. 0480-9722 can be used for mounting the bench version, 1157-B, in a standard rack.


Figure 1-1. 1157-B Scaler, showing controls, indicators, and connectors. Front view, above; rear view, below.


Table 1-1
CONTROLS, INDICATORS, AND CONNECTORS

| Fig. 1-1 Item No. | Name | Description | Function |
| :---: | :---: | :---: | :---: |
| 1 | INPUT | GR874® locking coaxial connector. | Input port; can be moved to rear panel. Impedance: $50 \Omega$; frequency: $1-500 \mathrm{MHz}$; level: 0.1-7 V rms. |
| 2 | INPUT LEVEL | Meter. | Indicates acceptable combination of input level and SENSITIVITY-control setting, when pointer is in green sector. |
| 3 | SENSITIVITY | 4-position rotary switch. | Attenuation of input signal; $0,6,14$, and 20 dB (voltage ratios 1, 0.5, 0.2, 0.1). Max sensitivity cw . |
| 4 | Pilot light | Flush round lamp. | Indicates when line power on. |
| 5 | MULTIPLY COUNTER READING BY | 3-position rotary switch. | Selects scale factor of main output frequency: 10 or 100. Turns line power OFF. |
| 6 | 10:1/100:1 OUT | BNC coaxial jack. | Main output port; can be moved to rear panel. Impedance: $50 \Omega$; frequency: $0.01-50 \mathrm{MHz}$; source level: 1-V pk; waveform: + pulse from $0-\mathrm{V}$ base line; duty ratios: $60 \%$ for 10:1, $40 \%$ for 100:1. |
| 7 | 100:1 SYNC OUT | BNC coaxial jack. | Auxilliary output port; can be moved to rear panel. Characteristics like item 6 except frequency: $0.01-5 \mathrm{MHz}$; duty ratio: 60\%. |
| 8 | Line-voltage switch " $50-400 \mathrm{~Hz}$ " | 2-position slide switch. | Accomodates power supply to linevoltage ranges: $100-125$ or $200-250 \mathrm{~V}$. |
| 9 | 1/10 A FUSE | Fuse in extractorpost holder. | Protects against overload damage when line voltage 230 V . |
| 10 | 2/10 A FUSE | Fuse in extractorpost holder. | Protects against overload damage when line voltage 115 V . |
| 11 | INPUT location | Mounting hole with cover plate. | Alternate location for Item 1. |
| 12 | OUT locations | Mounting holes. | Alternate locations for items 6 and 7. |
| 13 | Power plug | 3 -pin power plug. | Power-line connection, with ground. |

Table 1-2
ACCESSORIES AVAILABLE

| Tvpe and Name | Characteristic | Function |
| :---: | :---: | :---: |
| 1159 Recipromatic Counter | Autoranging, fast, programmable, sensitivity: 20 mV ; frequency: $0.6 \mathrm{~Hz}-20 \mathrm{MHz}$. | Frequency measurement, 6 -digit presentation. |
| 1191 Counter | Programmable, sens: 20 mV ; frequency: up to 35 MHz . | Frequency in 8 digits, period, interval, ratio. |
| 1192 Counter | Manual only, sens: 20 mV . frequency: up to 32 MHz . | Frequency in 7 digits, period, interval, ratio. |
| 1591 Variac® Automatic Voltage Regulator | Accuracy: $\pm 0.2 \%$, capacity: 1.0 kVA . | Line-voltage regulation without distortion. |
| 874-F185L Low-Pass Filter | Frequency: 185 MHz . | Eliminate miscounts due to harmonics. |
| 874-F500L Low-Pass Filter | Frequency: 500 MHz . | Eliminate miscounts due to harmonics. |
| 874-TPDL Power Divider | Coax. tee, matched impedance. | Low-VSWR signal branching. |
| 874-TL Tee | Coaxial. | Signal-path branching. |

Table 1-3
GR874® LOCKING ADAPTORS TO OTHER SERIES

| Mates | Type | $\begin{gathered} \text { Contains } \\ \text { GR874 and... } \end{gathered}$ | $\begin{gathered} \text { Connects } \\ \text { GR874 to... } \end{gathered}$ | Catalog Number |
| :---: | :---: | :---: | :---: | :---: |
| Type BNC | 874-OBJL | BNC Jack | BNC Plug | 0874-9701 |
| Type C | 874-QCJL | C Jack | C Plug | 0874-9703 |
| Type MICRODOT | 874-OMDJL | Microdot Jack | Microdot Plug | 0874-9721 |
| Type N | 874-QNJL | $N$ Jack | $N$ Plug | 0874-9711 |
| Type SC | 874-OSCJL | SC Jack | SC Plug (Sandia) | 0874-9713 |
| Type TNC | 874-QTNJL | TNC Jack | TNC Plug | 0874-9717 |
| GR900® Precision 14 -mm Connector | 874-0900L | GR900 | GR900 | 0874-9709 |
| Type SMA Miniature | 874-QMMJL | SMA Jack | SMA Plug | 0874-9723 |
| $\begin{aligned} & \text { AMPHENOL } \\ & \text { APC- } 7 \end{aligned}$ | 874-QAP7L | APC-7 | APC-7 Precision 7-mm Connector | 0874-9791 |

## Installation-Section 2

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Figure 2-1. Dimensions of 1157-B Scaler.

### 2.1 GENERAL.

The 1157-B Scaler, having half a standard rack width, is a compact instrument on the bench and makes a convenient combination with the 1192 Counter, side-by-side, either bench or rack mounted. Only ac line power and an input signal are required. Available are frequency-scaled outputs and (on the counter) a digital frequency readout.

### 2.2 POWER.

Power requirements are 14 W at 100 to 125 V or 200 to $250 \mathrm{~V}, 50$ to 400 Hz . A linevoltage switch (Figure 1-1, item 8) is provided on the rear panel of the instrument to convert from one line-voltage range to the other. Fuse A-F2, 0.1 A, is used for the 200- to $250-\mathrm{V}$ range; fuse $\mathrm{A}-\mathrm{F} 1$, 0.2 A , is used for the 100 - to $125-\mathrm{V}$ range (Figure $1-1$, item numbers 9 and 10 , respectively).

Make connection to the power line by means of three-wire power cord, supplied. Attach it to the power plug (Figure 1-1, item 13) on rear of instrument.

### 2.3 BENCH MODEL.

### 2.3.1 Dimensions.

The dimensions of the 1157-B in either available mounting configuration are shown in Figure 2-1. (Over-all height is reduced by 0.375 in . when feet are removed, as for rack installation.)

## NOTE

Dimensions are given in inches, with all fractions expressed as decimals to 3 places. The number of digits is not intended to be significant nor to indicate tolerance.


Figure 2-2. Method of mounting scaler in a relay rack.

### 2.3.2 Tilting.

The bench model can be tilted back, if desired for a better view of the panel, as follows: Pull the central part of the bail, which is pivoted at the front feet, down and forward. Let the bail support the front of the instrument. To return the bail to its storage position, push it back and up against bottom of cabinet.

### 2.4 RACK MOUNTING.

### 2.4.1 Single Instrument and Blank Panel (Figure 2-2).

The rack model of the 1157-B Scaler fits in any EIA standard RS-310 19-in. relay rack with universal hole spacing. This model, consists of the standard bench model and Rack Adaptor Set 0480-9722 (also available separately). Table 2-1 lists the parts included in that set. Conversion procedure is as follows:
a. Loosen the two captive 10/32 screws in the rear of the cabinet, near the sides, until instrument is free. Slide the instrument forward, out of its cabinet.
b. Remove the four feet from the cabinet. Simply push out the two rear feet. Spread the bail (A,Figure 2-2) slightly and the two front feet ( $B$ ) will drop out, releasing the bail. Be sure to save all parts for possible reconversion of instrument to bench mounting.
c. Push out the plugs from the four bosses (C) on the cabinet sides, near the front. Use a hammer and a small punch inside the cabinet to push each plug outward. Do not damage threads in the threaded holes.
d. Press the subpanel (D) into the blank panel (E), to form a liner for the latter.
e. Attach the short flange of the blank pane! near the front of the cabinet (on either side of cabinet, as desired)
using two 5/16-in. screws(F). Note that the screws enter in opposite directions - one from inside the cabinet and one from the flange side, as shown.
f . Push out the plug in the lower rear boss $(\mathrm{G})$ on the side toward the blank panel only, as in step c.
g. Attach one end of support bracket $(H)$ to the lower rear boss. The bracket must be placed so that the screw passes through a clearance hole, into a tapped hole. Lock the bracket in position with a 5/16-in. screw (J).
$h$. Attach the other end of the support bracket to the lower, rear hole in the wide flange, as shown, using a 5/16-in. screw (K).

Table 2-1
RACK ADAPTOR SET, 0480-9722

| Fig. 2-2 Item | No. <br> Used | Name | GR Part No. |
| :---: | :---: | :---: | :---: |
| E | 1 | Blank panel | 0480-8932 |
| D | 1 | Sub panel | 0480-8952 |
| Q | 2 | Rack adaptor assembly | 0480-4902 |
| H | 1 | Support bracket | 0480-8524 |
| - | 1 | Hardware set includes: | 0480-3080 |
| $\begin{aligned} & \text { F, J, K, } \\ & \mathrm{L}, \mathrm{M} \\ & \mathrm{~N} \end{aligned}$ |  | 8 Screws, Phillips head, 10-32, 5/16 in; 4 Screws, Phillips head, 10-32, 9/16 in., with captive nylon cup washers. |  |

## 2-2 INSTALLATION

i. Attach one rack adaptor assembly ( Q , including handle) to the side of cabinet opposite the blank panel, using two $5 / 16$-in screws (L). Again, note that the screws enter in opposite directions, one from inside the cabinet and one from outside. Use the upper and lower holes in the assembly.
j. Attach the other rack adaptor assembly ( Q , including handle) to the wide flange on liner ( $D$ ) and the flange on blank panel (E). Use two 5/16-in. screws (M) through the two flange holes that are nearest the panel and through the upper and lower holes in the assembly. Again, the screws enter in opposite directions.
k. Install the instrument in its cabinet and lock it in place with two captive rear-panel screws that were loosened in step a.
I. Place a straight edge across instrument panel and blank panel. Loosen screw(J) through the slot in support bracket $(H)$. Exert a slight pressure on blank panel (E) so that it forms a straight line with the instrument panel, and tighten screw (J), to lock the panels in this position.
m . Slide the entire assembly into the relay rack and lock it in place with four $9 / 16$-in. screws ( $N$, with captive nylon cup washers). Use two screws on each side and tighten them by inserting a screwdriver through holes $(P)$ in the handles.

### 2.4.2 Reconversion to Portable Bench Mounting.

To reconvert the instrument for bench use, reverse the procedures of paragraph 2.4.1, first removing the entire assembly of instrument, cabinet, and blank panel from the rack.
a. Remove the instrument from its cabinet.
b. Remove support bracket (H) from the cabinet (Figure 2-2).
c. Remove the blank panel ( E , with handle attached) from one side of cabinet.
d. Remove the rack adaptor set (handle) from the other side of cabinet.
e. Push the two rear (rubber) feet into the cabinet; slide bail ( $A$ ) and two front feet ( $B$ ) into place.
f. Install the instrument in its cabinet and lock it in place with the two captive screws through rear panel (Figure 1-1).

### 2.4.3 Rack-mounting Two Instruments.

Two instruments of the same panel size (such as two scalers or one scaler and one 1192 Counter) can be mounted side-by-side in a standard $19-\mathrm{in}$. relay rack. Use the procedure of paragraph 2.4.1, substituting the second instrument for the blank panel. Do not use the support bracket (H, Figure 2-2), but insert three screws through the bosses in the adjacent sides of the cabinets, two near the front (C) and one near the rear (G). The four feet and the bail must, of course, be removed from each cabinet. Use the four screws ( $N$ ) with nylon washers to lock the instruments in the rack. The required hardware includes 2 of item $\mathrm{Q}, 3$ of $J$, and 4 of $N$ (Table 2-1).

### 2.5 OPTIONAL CONNECTOR LOCATIONS.

The INPUT connector is normally mounted on the front panel (Figure 1-1) but can be moved to the rear as follows:
a. Remove the scaler from its cabinet after loosening 2 captive screws at the rear, near left and right sides.
b. Remove four screws that secure the connector to the front panel.
c. Remove the corresponding cover plate from the rear panel.
d. Move the connector to the rear, reinsert its screws, and secure in place.

## NOTE

Mate another locking GR874 connector into this unit before tightening the screws, to ensure proper centering.
e. Install the cover plate in the vacant location on the front panel. Use the accompanying screws, lockwashers, and nuts.

The 10/100 OUT or SYNC OUT connector (or both) can also be moved to the rear as follows:
a. Remove the scaler from its cabinet, as before.
b. Unsolder the coaxial cable from connector and ground lug. Remove nut, lockwasher, and lug (inside); retain the spacer ring (outside).
c. Remount connector in the rear location having the appropriate label. Use all the hardware, in original sequence.
d. Resolder the cable to connector and ground lug, after appropriate changes in route through cable clamps.

### 2.6 INTERCONNECTIONS.

Use an appropriate patch cord (Table 2-2) to connect the signal to be measured to the INPUT connector. Connect the 10/100 OUT port of the scaler to the input port of a counter or other frequency-measuring instrument. The following choices of patch cords are appropriate for the corresponding counters: GR 0776-2000 for the 1192, 776-B for the 1159, and 776-C for the 1191 Counter.

### 2.7 ENVIRONMENT.

The scaler will operate reliably with ambient temperatures between $0^{\circ}$ and $55^{\circ} \mathrm{C}\left(32^{\circ}\right.$ to $\left.131^{\circ} \mathrm{F}\right)$.

### 2.8 LINE-VOLTAGE REGULATION.

The accuracy of measurements accomplished with precision electronic test equipment operated from ac line sources can often be seriously degraded by fluctuations in primary input power. Line-voltage variations as much as $\pm 5 \%$ are commonly encountered, even in laboratory environments. Although most modern electronic instruments incorporate some degree of regulation, possible powersource problems should be considered for every instrumentation setup. The use of line-voltage regulators between
power lines and the test equipment is recommended as the only sure way to rule out the effects on measurement data of low line voltage, transients, and other power phenomena.

The General Radio Type 1591 Variac® Automatic Voltage Regulator is a compact and inexpensive equipment capable of holding ac line voltage within $0.2 \%$ accuracy for input ranges of $\pm 13 \%$. It will assure that the scaler, rated for 100-125 (or 200-250) V , can be operated reliably in spite
of input transients in the range $85-140$ (or 170-280) V. The $1-k V A$ capacity of the 1591 will handle a rack full of solid-state instrumentation with no distortion of the input waveform. This rugged electro-mechanical regulator comes in bench or rack-mount versions, each with sockets for standard 2- or 3-wire instrument power cords.

Further details can be found in your GR catalog or in the GR Experimenter for October, 1967.

Table 2-2
AVAILABLE INTERCONNECTION ACCESSORIES


## Operation-Section 3

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### 3.1 PRELIMINARY CHECKS.

Make the following checks before operating the scaler:
a. Check that the line-voltage switch (item 8, Figure 1-1) is positioned according to the available power-line voltage.
b. Connect the power plug (item 13, Figure 1-1) to a suitable power line, using the power cord supplied.
c. Turn the MULTIPLY... BY switch cw from OFF and check that the pilot light goes on (item 4).

### 3.2 GENERAL OPERATION.

Refer to paragraph 1.3 for a description of controls, indicators, and connectors. Proceed as follows:
a. Turn the MULTIPLY . . BY switch to 100. The pilot light should glow.
b. Set the SENSITIVITY control ccw, to the least sensitive position.
c. Verify that the level of signal to be measured is less than 7 V rms into a $50-\Omega$ load. Couple to the INPUT connector, using a patch cord selected from tables in paragraph 1.5.
d. Adjust the SENSITIVITY control as required to bring pointer into green segment of INPUT LEVEL meter. If two positions satisfy, use the one closer to a midscale reading.
e. Connect from the $10 / 100$ OUT jack to a counter, scope, or other frequency-measuring instrument (as described in paragraph 2.6).
f. Multiply the indicated frequency by the scale factor, 100 , to complete the measurement.


Figure 3-1. Typical scaler input sensitivity.


Figure 3-2. Use of scaler to trigger a scope.
g. If a scale factor of 10 is preferred, turn the MULTIPLY . . . BY switch to 10.
h. Obtain a coherent pulse-type signal at $1 / 100$ the input-signal frequency from the SYNC OUT jack (for triggering a scope or controlling a gate independently of the main output circuit).

### 3.3 TERMINAL CHARACTERISTICS.

### 3.3.1 Input.

Frequency: $1-500 \mathrm{MHz}$.
Impedance: $50 \Omega$.
Attenuator: 1-2-5-10 sequence (voltage), i.e., 0-6-14-20 dB.

Maximum safe level: 7 V rms.
Sensitivity: better than $0.1 \mathrm{Vrms}(0.3 \mathrm{~V} \mathrm{pk}-\mathrm{pk})$; see Figure 3-1.
Coupling: ac ( $0.01 \mu \mathrm{~F}$ series capacitor).

### 3.3.2 Outputs.

Frequency: $0.01-50 \mathrm{MHz}$.
Impedance: $50 \Omega$.
Level: at least 1 Vpk , source voltage.
Waveform: positive pulses.
Coupling: direct.

### 3.4 APPLICATIONS.

### 3.4.1 Counter Range Extension.

Extension of the upper frequency limit of any modern counter, by a factor of either 10 or 100 is limited only by the scaler input-terminal characteristics. The frequency readout must be interpreted; move the decimal point as shown explicitly by the MULTIPLY COUNTER READING BY switch.

Accuracy of measurement is unaffected by the scaler. Counter accuracy is usually specified as reference-oscillator stability $\pm 1$ count (at the counter input). That 1 count is 10 or 100 cycles of the signal at scaler INPUT. For increased resolution in any given measurement, increase the counter's gate time.

The upper frequency limit of other frequency-measuring instruments is similarly extended, instruments like analog frequency meters, discriminators, and scopes.

The recommended companion for this scaler is the compact, inexpensive, general purpose 1192 Counter.

### 3.4.2 Scope Trigger.

Use the scaler to process the trigger signal for an oscilloscope if its sweep circuitry is inadequate to do so directly. Often a signal within the bandwidth capability of the vertical amplifier is too fast for reliable triggering. When divided coherently by the scaler, that signal provides an ideal trigger.

Use the scaler-triggered time base to advantage (even at low frequencies) whenever the device under test involves delays that are large compared to a signal period. Such a time base may be particularly useful if the device is a digital processor such as a divider. The signal driving the scaler should be unchanged by the experiment, as suggested in the diagram of Figure 3-2.

### 3.4.3 Filtering.

If the signal to be measured has harmonic distortion or higher-frequency noise with it, use a low-pass filter at the INPUT port to improve reliability and significance of measurements. Two suitable filters, with cutoff frequencies of 500 and 185 MHz , respectively, are listed in paragraph 1.5.

## Theory-Section 4

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Figure 4-1. Block diagram of 1157-B Scaler.

### 4.1 GENERAL.*

Theory is discussed first by an explanation of the main functions, with reference to a block diagram. Then individual circuits are described, in greater detail. Circuits designated $A, B, C, D$, and $V$ are the over-all assembly with panel wiring, 3 signal-processing boards, and the powersupply board, respectively.

## NOTE

Each reference designator used in our schematic diagrams and circuit descriptions now includes an initial letter, before a hyphen, to identify the subassembly. The numeric portion of each designator is generally shorter than would be

[^0]the case if a block of numbers were assigned to each subassembly. A new designation WT (wiretie point) replaces the customary AT (anchor terminal). The letter before the hyphen may be omitted only if clearly understood, as within a subassembly schematic diagram.
Examples: $\mathrm{B}-\mathrm{R} 8=\mathrm{B}$ board, resistor 8; D-WT2 $=$ D board, wire-tie point 2; CR6 on the $V$ schematic is a shortened form of V -CR6 $=\mathrm{V}$ board, diode 6. The instrument may contain A-R1, B-R1, C-R1, and D-R1.

### 4.2 BLOCK FUNCTIONS (Figure 4-1).

The scaler accepts an essentially single-frequency input signal and provides an output suitable to drive a counter at $1 / 10$ or $1 / 100$ of the input frequency. Discussion of internal functions is related to the block diagram.

### 4.2.1 Attenuator - A.

A switched resistive network provides 4 steps of input-signal attenuation to accomodate large signal levels, feeding an appropriate fraction to the sensitive, very broad-band input amplifier.

### 4.2.2 Meter Drive - B.

A stable metering circuit provides visual indication of signal level ahead of the input amplifier, to assist the operator in setting the attenuator properly.

### 4.2.3. Input Amplifier - B.

The input amplifier accepts signals in the ranges 1-500 MHz and 0.1-0.7 V . It provides gain, impedance transformation, and isolation ahead of the divider circuitry.

### 4.2.4 Pulse Generator - C.

Ahead of the first divider is a generator which produces one very sharp negative pulse per cycle of the input signal.

### 4.2.5 Binary Divider - C.

A very fast divider switches from one stable state to the other each time it receives a pulse. The resulting square wave, at $1 / 2$ the input frequency, passes through a buffer amplifier on its way to subsequent dividers.

### 4.2.6 By-5 Divider - D.

A fast switching circuit divides further, to $1 / 10$ the input frequency. One output channel goes through a buffer amplifier and selector switch to the 10/100 OUT jack. The other drives the subsequent divider.

### 4.2.7 By-10 Divider - D.

The final two steps of division, by 2 and 5 , produce the output signal at $1 / 100$ the input frequency. This signal passes through buffer channels to the 10/100 OUT jack (through the selector switch) and to the SYNC OUT jack.

### 4.3 CIRCUIT DESCRIPTION.

### 4.3.1 Over-all Assembly - A (Figure 6-3).

The attenuator is built around the SENSITIVITY switch A-S3. Each step selects a completely separate resistive pi
network, the last one being the degenerate form, a single wire. Input impedance remains $50 \Omega$ in all positions.

The other front-panel switch, MULTIPLY ... BY, has two parts, A-S1 and A-S2. The latter selects either of the optional signals, 10:1 or 100:1, for the main output jack A-J3. In the OFF position it selects neither, and A-S1 opens the power line.

The ac power circuit includes a line voltage switch A-S4, which connects A-T1 dual primary windings in parallel or series for nominally 115 or $230-\mathrm{V}$ lines. The appropriate fuse is automatically connected when A-S4 is in the correct position.

### 4.3.2 Input and Metering - B (Figure 6-6).

The input amplifier, 3 direct-coupled stages, incorporates high-frequency transistors and suitable compensation to obtain the necessary sensitive, broad-band performance. Gain is approximately 12 dB .

The meter-drive circuit uses an analog integrated-circuit amplifier B-IC1 to furnish meter A-M1 with 250 to $750 \mu \mathrm{~A}$ (the range of the green sector) for 100 to 700 mV of signal level at the input B-J1 (after the attenuator).

Diode B-CR1 serves as a peak detector. Diode B-CR2, carrying a small forward current, is used to subtract the initial forward voltage drop from the detector output, so that the transfer characteristic is nearly linear.

The gain of the meter-drive amplifier is switched by diode B-CR3. The diode is open, making gain higher, for signals $0-100 \mathrm{mV}$ at $\mathrm{B}-\mathrm{J} 1$. The diode conducts, making gain lower, for larger signals. The resistive network not only sets these gains to provide the correct meter currents (250 and $750 \mu \mathrm{~A}$ ) for the accepted signal range, but also ensures that a safe overload current ( $1200 \mu \mathrm{~A}$ ) follows from any large signal that saturates the amplifier.

### 4.3.3 Trigger - C (Figures 4-2, 6-7).

The trigger generator processes the incoming signal to supply a negative pulse to the binary divider. These circuits incorporate tunnel diodes, whose general characteristics are shown in Figure 4-2.


Figure 4-2. Tunnel-diode characteristics.

Load lines are drawn for a given resistance $R=V_{3} / I_{3}$. Notice that when $V=V_{3}$, there are 2 possible equilibrium conditions, $C$ and $G$ ( $E$ is unstable). If $V$ increases, the sequence of stable conditions is $A, B, C, D, H, J$, with a very rapid transition from $D$ to $H$. Conversely, the sequence is $J, H, G, F, B, A$, with a very rapid transition from $F$ to $B$. These rapid transitions between high and low voltage states (and the exclusion of any intermediate state) make tunnel diodes useful for sharpening the rise-time of a pulse or making a fast flip-flop. The low dynamic impedance of the regions above and below the transition region make tunnel diodes useful also as limiters.

Tunnel diode C-CR1 is driven far enough to change state and reverse every cycle of the input signal. (There must not be enough noise or harmonic distortion to cause extraneous reversals.) With series resistor C-R1 to absorb the voltage peaks, the signal at $\mathrm{C}-\mathrm{Q} 1$ base is therefore nearly square. The rise D-H (Figure 4-2) is particularly sharp; the fall is rounded at H-F before the sharp drop F-B.

Tunnel diode C-CR2 functions similarly, except that the waveform has been inverted by C-Q1. The sharp transition is further emphasized and so is the limiting action. Transistor C-Q2 amplifies and inverts again to produce a square wave with a very steep positive leading edge.

Pulse generator $\mathrm{C}-\mathrm{Q} 3$ is turned on abruptly by this step, but conducts strongly for only a small fraction of a nanosecond thereafter, because the emitter bypass C-C11 is so small. Consequently the C-O3 collector waveform is a short negative pulse, once each cycle of the main input signal.

### 4.3.4 Binary Divider - C (Figure 6-7).

The binary incorporates a bridge with tunnel diode pair C-CR3/C-CR4 on one side, a resistor pair opposite, and an inductor across the middle. Normally, the voltage across the bridge is about 0.5 V , enough to allow one diode to be in its high-voltage state and one low, but not both in the same state. The network also restricts the "high" diode to a lower current than its twin. (Suppose C-CR3 is in the high-voltage state; C-R24 is forced to a larger IR drop than C-R25; therefore current flows through C-L1, adding with C-CR3 current to give C-CR4 more current although its voltage is lower.)

The negative pulse applied to this bridge drops whichever diode was high into the low-voltage state. Then both tunnel diodes cycle momentarily below point B (Figure 4-2). After the pulse, whichever diode was low is the first to reach point $D$ and switches to the high-voltage state, "taking turns." Memory is provided by inductor C-L1. (Continuing the above supposition, enough inductor current is still flowing during and shortly after the pulse to give C-CR4 more current than C-CR3.)

The signal out of this divider, then, is a square wave at half the frequency of the input signal. A 3-stage buffer amplifier (C-Q4, -Q5, and -Q6) follows the binary divider and drives the following stage.

### 4.3.5 By-5 Divider - D (Figures 4-3, 6-11).

A set of 3 integrated-circuit flip-flops is arranged with feedback to make a fast scale-of-5 divider. Each flip-flop has these properties, using positive logic: •
a. In the 1 state, output Q is $1, \overline{\mathrm{Q}}$ is 0 .
b. In the 0 state, output $Q$ is $0, \overline{\mathrm{Q}}$ is 1 .
c. Application of a + clock pulse at input C causes the flip-flop to assume the state of input $D$.
d. Application of $a+$ pulse at input $R$ resets the flip-flop to the 0 state.

The time sequence is shown in Figure 4-3. Start with a time when all 3 flip-flops are in the 0 state. The signal at D-J1 (having come through the binary divider) is used as the clock drive. (Abbrev. used: IC1, IC2 . . . for D-IC1, D-IC2 . . .)

1. First clock pulse sets IC1 to 1 because its input $D$ is 1, obtained from $\overline{\mathrm{Q}} / \mathrm{IC} 3$.
2. Second clock pulse sets IC2 to 1 because its input $D$ is 1 , obtained from $\mathrm{Q} / \mathrm{IC} 1$.
3. Third clock pulse sets IC3 to 1 because its input $D$ is 1, obtained from Q/IC2.
4. Fourth clock pulse sets IC1 to 0 because its input $D$ is 0 ( $\overline{\mathrm{Q}} /$ IC3 was made 0 by step 3).
5. Fifth clock pulse sets IC2 to 0 because its input $D$ is 0 , as a result of step 4.
6. A chain reaction sets IC3 to 0 because its input $R$ becomes 1 with $\overline{\mathrm{Q}} / \mathrm{IC} 2$, as a result of step 5 . Notice that IC3 being reset before the next clock pulse makes the divider scale by 5 instead of 6 .
7. Sixth clock pulse will act exactly like the first because all 3 flip-flops are in the 0 state. Therefore, the dividing cycle repeats with every 5 clock cycles, i.e., every 10 cycles of the input signal.

A difference amplifier, D-Q1/D-Q2, serves as a buffer for the $\div 10$ output, available at the $10 / 100$ OUT jack when the MULTIPLY... BY selector is set to 10 . The phase of this output is the same as that of $\overline{\mathrm{Q}} / \mathrm{IC} 3$, and the duty ratio is likewise $60 \%$.


Figure 4-3. By-5 divider timing diagram.

### 4.3.6 By-10 Divider - D (Figures 4-4, 6-11).

An IC binary divider and another scale-of-5 circuit accomplish the decade division. A final buffer amplifier follows.

The binary IC4 has the property that each + pulse applied simultaneously to inputs $J$ and $K$ reverses the state of its internal flip-flop. Its output Q/IC4 is a square wave at half the frequency of the $\div 10$ output (at D-J2). Difference amplifier D-Q3/D-Q4 acts as a "clock" driver for the following divider. (See Figure 4-4, first 2 waveforms.)

Division by 5 takes place in D-IC5 and D-IC6 with logic very similar to that described in paragraph 4.3.5. D-1C5 contains flip-flops $A$ and $B$, analagous to $D-I C 1$ and $D-I C 2$; D-IC6 is comparable to D-IC3. These flip-flops have the following properties, using positive logic:
a. In the 1 state, output Q is $1, \overline{\mathrm{Q}}$ is 0 .
b. In the 0 state, output Q is $0, \overline{\mathrm{Q}}$ is 1 .
c. Application of $a$ - pulse at input $C$ causes the flip-flop to assume the state of input $J$, provided that input $K$ is always driven opposite to J . (If both J and K were 0 , no change would occur; if both were 1 the flip-flop would switch state.)
d. Application of a - pulse at input $R$ resets the flip-flop to the 0 state.

The timing sequence is shown in Figure 4-4. Start with a time when all 3 flip-flops are in the 0 state. The clock drive, from D-Q3 collector, is applied to all 3 flip-flops at their C terminals. (Abbrev. used: IC4, IC5 . . . for D-IC4, D-1C5 . . .)

1. Clock pulse C 1 sets IC5A to 1 because its $\mathrm{J} / \mathrm{K}$ inputs are $1 / 0$, determined by IC6.
2. Clock pulse $C 2$ sets IC5B to 1 because its $J / K$ inputs are $1 / 0$, determined by IC5A.

3. Clock pulse C3 sets IC6 to 1 because its $J / K$ inputs are $1 / 0$, determined by IC5B.
4. Clock pulse $C 4$ sets IC5A to 0 because its $J / K$ inputs are $0 / 1$, determined by IC6.
5. Clock pulse $C 5$ sets IC5B to 0 because its J/K inputs are $0 / 1$, determined by IC5A.
6. A chain reaction sets IC6 to 0 because its input $R$ becomes 0 with $\mathrm{Q} / \mathrm{IC} 5 \mathrm{~B}$, as a result of step 5 . Notice that IC6 being reset before the next clock pulse makes the divider scale by 5 instead of 6 .
7. Clock pulse C 6 will act exactly like C 1 because all 3 flip-flops are in the 0 state. Therefore, the dividing cycle repeats with every 5 clock cycles, i.e., every 100 cycles of the signal at the INPUT connector.

A difference amplifier, D-Q5/D-Q6, serves as a buffer for the $\div 100$ outputs. D-J4 supplies the SYNC OUT signal, which has a $60 \%$ duty ratio. D-J3, with the complementary signal $-40 \%$, is connected to the $10 / 100$ OUT jack when the MULTIPLY ... BY selector is set to 100 .

### 4.3.7 Power Supply - V (Figure 6-10).

The $+20-\mathrm{V}$ section is nearly independent of the $-20-\mathrm{V}$ part, the former using rectifier diodes V-CR1 and -2, its own regulator, and current limiter. Filtering action by A-C1 is shared with $-20-\mathrm{V}$ supply. Cascode series regulator $\mathrm{V}-\mathrm{Q} 1 / \mathrm{V}-\mathrm{Q} 2$ is driven by $\mathrm{V}-\mathrm{Q} 4$ in the required sense to hold the output voltage constant at wire-tie point V-WT6. Normally, V-O4 is turned mildly on with a base-emitter bias of 0.6 V , the tap on V -R5 "set $20 \cdot \mathrm{~V}$ " being that much above the potential across Zener-diode V-CR9, when the output terminal V -WT6 is +20 V above ground. V - Q 3 is a current limiter that, if turned on by excessive IR drop in V -R3, will partially starve the base of $\mathrm{V}-\mathrm{Q} 2$ and so protect the power supply from damage by a short circuit.

The $-20-\mathrm{V}$ section is dependent on the $+20-\mathrm{V}$ regulator for reference voltage. It uses rectifier diodes V-CR3 and -4, filter capacitor A-C1 (part of which is shared), a separate regulator, and limiter. Cascode series regulator V-Q7/V-Q8 is driven by V - Q 5 in the proper sense to hold the output voltage at V-WT7 constant. Normally, V-Q5 is turned mildly on with an emitter-base bias of 0.6 V when V -WT7 voltage is $-20 \mathrm{~V} . \mathrm{V}$-Q6 is a current limiter that, if turned on by excessive IR drop in V-R9, will partially starve the base of V-Q7.

The $5.25-\mathrm{V}$ section also depends on the $+20-\mathrm{V}$ regulator for reference. Cascode series regulator V-Q9/V-Q10 is driven by V-Q12 so that the output voltage at V-WT12 stays constant. Normally, V-Q12 has a base-emitter bias of 0.6 V when V -WT12 voltage is +5.25 V . V -Q11 is a current limiter that, when turned on by excessive $I R$ drop in V-R10, will partially starve the base of V-Q10.

Figure 4-4. By-10 divider timing diagram.

## Service and Maintenance-Section 5

5.1 GR FIELD SERVICE ..... 5-1
5.2 MINIMUM PERFORMANCE STANDARDS ..... 5-1
5.3 DISASSEMBLY AND REASSEMBLY ..... 5-3
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Figure 5-1. Generalized test setup.

### 5.1 GR FIELD SERVICE.

The two-year warranty attests the quality of materials and workmanship in our products. When difficulties do occur, our service engineers will assist in any way possible. If the difficulty cannot be eliminated by use of the following service instructions, please write or phone the nearest GR service facility (see back page), giving full information of the trouble and of steps taken to remedy it. Describe the instrument by type number (front panel), serial, and ID numbers (rear panel).

Before returning an instrument to General Radio for service, please ask our nearest office for a "Returned Material"number. Use of this number in correspondence and on a tag tied to the instrument will ensure proper handling and identification. For instruments not covered by
the warranty, a purchase order should be forwarded to avoid unnecessary delay.

For return shipment, please use packaging that is adequate to protect the instrument from damage, i.e., equivalent to the original packaging. Advice may be obtained from any GR office.

### 5.2 MINIMUM PERFORMANCE STANDARDS.

### 5.2.1 General. Figure 5-1.

The significant aspects of performance are flawless scaling over the specified frequency range, input sensitivity, and output level.

The test setup is shown in Figure 5-1. Recommended test equipment is listed in Table 5-1. The requirements given are significant ones, but may not be a complete and

Table 5-1 TEST EQUIPMENT

| Item | Requirements | Recommended Type* |
| :---: | :---: | :---: |
| Signal generators | Frequencies: $1-500 \mathrm{MHz}$; with $\pm 0.5 \%$ accuracy; levels: $0.1-3 \vee$ into $50 \Omega$. | GR 1003 and GR 1026 |
| Oscilloscope | Bandwidth: dc-1 GHz; deflection factor: 2-200 mV/div; time base: $0.2 \mathrm{~ns}-1 \mu \mathrm{~s} / \mathrm{div}$; | Tektronix 561 with 3S1 and 3T77A plug-in units. |
| Oscilloscope | Bandwidth: dc - 50 MHz ; deflection factor: $5 \mathrm{mV}-10 \mathrm{~V} /$ div. | Tektronix 453 with P6008 probe. |
| Counter | Frequency range: up to 30 MHz ; input impedance: 50 digits: 6 or 7 preferred, 5 min . | GR 1192 |
| Scaler | Same as scaler being tested. | GR 1157-B |
| Electronic multimeter and tee connector. | Voltage range: $0.01-30 \mathrm{~V}$; accuracy: $\pm 2 \% \mathrm{dc}, \pm 10 \%$ at 500 MHz ; ohmmeter accuracy: $\pm 5 \%$; test voltage: 1.5 V . | GR 1806 with 1806-P1. |
| Line-voltage regulator | Stability: $\pm 0.2 \%$, capacity: 1 kVA ; adjustment: 105-125 V. | GR 1591 |
| Autotransformer, adjustable and metered. | Current rating: 5 A ; meter accuracy, watts and volts: $\pm 3 \%$. | GR W5MT3W Variac® |
| Adaptor | GR874 to Microdot plug. | GR874-OMDP |
| Patch cords (2) | GR874 each end. | GR874-R22A |
| Patch cords (2) | BNC plug each end. | GR 776-C |
| Patch cord | GR874 to BNC plug. | GR 776-B |
| Capacitor | Dc blocking, coaxial. | GR874-K |
| Power Divider | VSWR: $<1.06$, dc- $0.5 \mathrm{GHz} ;$ <br> insertion loss: $6 \mathrm{~dB}(+2,-0.5 \mathrm{~dB})$ to each output. | GR874-TPD |

[^1]sufficient set of specifications for choosing substitutes for the recommended types.

### 5.2.2 Basic Operation and Sensitivity.

a. Set each signal generator to provide 0.2 V cw into a $50-\Omega$ load, so that each in turn will drive the scalers at a $0.1-\mathrm{V}$ level; or if only one scaler is available, omit the power-divider tee and set the signal generators to 0.1 V .
b. Connect the oscilloscope channels 1 and 2 from the outputs of the scaler under test. Set its MULTIPLY . . . BY switch to 10.
c. Set input frequency to 100 MHz .
d. Verify that the INPUT LEVEL meter points to the left end of its shaded zone, with clockwise setting of the SENSITIVITY switch.
e. Verify on the scope that the output level is at least 1 $\checkmark$ pk-pk on each channel. (The scaler is driving a high impedance load.)
f. Verify on the scope that the output periods are 10 and 100 times the input period, i.e., 0.1 and $1 \mu$ s for a $100-\mathrm{MHz}$ input.
g. Repeat steps e and f, for these input frequencies: 1, $10,(100$ already done) and 500 MHz .

### 5.2.3 Scaling, Method 1.

## NOTE

This method is satisfactory. However, the alternative, method 2, is much preferred if a second scaler is available. It may be part of a GR 1192-Z Counter ( 500 MHz ).
a. Connect the 100:1 SYNC OUTPUT of the scaler to the counter. Set its gate and display times each to 1 s .
b. Verify that the counter reads $1 \%$ of the signalgenerator frequency ( 500 MHz ), within $\pm 0.5 \%$.
c. Change the frequency slowly (over several counts) to 450 MHz , keeping a watch for gross errors in counting.
d. Repeat step b at intervals of 50 MHz down to 50 MHz and also check at 1 MHz . During each transition except the last one, watch the counter, as in step c.
e. If a frequency is found where a gross error in counting occurs (step b is not verified) within the specified range of inputs for the 1157-B, the counter has failed.
f. Repeat steps a-e for these input levels ( 0.1 V already done): 0.316, and 1 V , i.e., for signal-generator OUTPUT RANGE steps of 10 dB .

### 5.2.4 Scaling, Method 2.

a. Connect the 100:1 SYNC OUTPUT of the scaler under test to channel $A$, that of the auxilliary scaler to channel $B$ of the counter.
b. Set the counter controls to measure RATIO for 100,000 PERIODS, and to hold the DISPLAY for 10 ms , in the STORAGE mode. (With a 5-digit counter use 10,000 periods.)
c. Sweep the frequency $1-500 \mathrm{MHz}$ in any convenient bands at a rate not exceeding one octave (or one band of the GR 1026) in 10 seconds. Any band of special interest may be explored at any lower sweep rate, down to zero.
d. Verify that the ratio is always $1.00000 \pm .00002$ (except when the count is interrupted by bandswitching). (Read $1.0000 \pm .0002$ on 5 -digit counters.)

## NOTE

There may be no decimal point displayed by a counter measuring ratio. Assume that the decimal point is in the 5th (4th) position from the right when measurement lasts $100,000(10,000)$ periods.
e. Repeat steps $c$ and $d$ for these input levels $(0.1 \mathrm{~V}$ already done): 0.316 and 1. V, i.e., for signal-generator OUTPUT RANGE steps of 10 dB .

### 5.3 DISASSEMBLY AND REASSEMBLY.

### 5.3.1 Cabinet.

Loosen the 2 captive screws in rear panel, one near each side, to release the instrument chassis. Slide instrument forward out of cabinet, whether rack or bench mounted. Reassemble by reversing this procedure.

### 5.3.2 Knobs.

## CAUTION

Do not use a screwdriver or other tool to pry off the knob if it is tight. Do not lose the spring clip in the knob while it is off.

To remove the knob from a front-panel control, to replace a damaged knob or the associated control, proceed as follows:
a. Grasp the knob firmly with dry fingers, close to the panel, and pull the knob straight away.
b. Observe the position of the setscrew in the bushing when the control is fully ccw.
c. Release the setscrew with an Allen wrench; pull the bushing off the shaft.

## NOTE

To separate bushing from knob, if for any reason they should be combined off of the shaft, drive a machine tap a turn or two into the bushing to provide sufficient grip for easy separation. To return the spring clip, if that falls out, install it in interior groove; push its curved flange into small slit in wall of knob.


Figure 5-2. Interior top view.

Reassembly procedure follows:
d. Slip bushing on shaft and rotate to correct position as observed in disassembly.
e. Keep bushing away from panel by at least the thickness of a filing card. Pull it out farther if necessary to prevent tip of shaft from protruding.
f. Tighten the setscrew in the bushing.
g. Place knob on bushing with spring clip opposite the setscrew.
h. Push knob on until it bottoms, then pull it slightly, to check that spring clip engages groove in bushing. Knob should clear panel without touching.

### 5.3.3 Etched-Circuit Boards.

Removal of an etched board, for replacement or repair, is done as follows:
a. Disconnect each coaxial cable (if any) by unscrewing the outer shell of miniature connector and gently pulling up.
b. Disconnect each soldered wire by unsoldering. Do not overheat etched board. (If V -board is involved, use this checklist: 5 transformer leads, 2 braided-cable wires, 5 links to other boards, and 4 to nearby capacitors.)
c. Remove screws at corners of board and lift it out. (If V-board is involved, it may be necessary to temporarily unfasten power transformer - 5 screws - to gain access.)

The part number of each replacement board, complete with all parts and checked for performance, appears with the drawing of the board, near the corresponding schematic diagram in Section 6.

### 5.3.4 Individual Parts.

Specific instructions in paragraphs 5.7 explain which boards may be repaired. Removal of a faulty part requires care. The board is liable to be damaged by heating much above the melting point of solder or by pulling a part still attached, in any way, to the copper foil conductor. Use a suitable tool to suck molten solder away. Be sure holes are clear before inserting new parts.

### 5.4 ADJUSTMENTS.

The internal adjustments may each be made with a small screwdriver, at points shown in Figure 5-2.

### 5.4.1 Set Meter - B-R5.

If meter needs calibration, supply INPUT with a sinusoidal signal of $0.10 \mathrm{~V} \mathrm{rms}$,100 MHz , and adjust B-R5 until pointer indicates left edge of green sector of INPUT LEVEL meter.

### 5.4.2 Pulse-Gen Bias - C-R9.

Adjust only with reference to instructions in paragraph 5.5.5. This sets the bias on tunnel diode C-CR2 for optimum drive into the pulse generator, and is most critical at highest frequencies.

### 5.4.3 Binary Bias - C-R19.

Adjust only with reference to instructions in paragraph 5.5.5. This sets the bias across the binary divider (tunneldiode bridge) for optimum performance, insensitive to noise, at all input frequencies.

### 5.4.4 Bias - D-R1.

Adjust only with reference to instructions in paragraph 5.5.6. This sets the dc component of the "clock" pulse train applied to the scale-of-5 divider.

### 5.4.5 Set 20 V - V-R5.

Adjust only with reference to paragraph 5.5.1 This sets the $+20-\mathrm{V}$ regulator.

### 5.5 TROUBLE ANALYSIS.

Trouble analysis of the 1157-B Scaler is based on the functional block diagram of Figure 4-1. If the scaler falls short of the minimum performance standards given in paragraph 5.2, return the instrument to General Radio Company for service or proceed as follows to make whatever analysis and adjustment are feasible. If the fault can be localized to one etched board, time can be saved. A spare board may be substituted while the old one is
returned to General Radio for repair. If adjustment is required upon such replacement, it is described in the following paragraphs.

### 5.5.1 Power Supply.

This procedure is to check the power supply for proper terminal voltages, to localize any fault, and to make pertinent adjustments. Complete this paragraph before making further trouble analysis.
a. Remove the cabinet.
b. Place controls in standard positions: SENSITIVITY, fully cw; MULTIPLY . . . BY, set at 100.
c. With the voltmeter ground terminal connected to WT2, verify the following dc voltages; refer to Figures 5-3 and 6-10:

$$
\begin{gathered}
\text { at } W T 6,+20 \mathrm{~V} \pm 1 \mathrm{~V} . \\
\text { at } \mathrm{WT7},-20 \mathrm{~V} \pm 1 \mathrm{~V} . \\
\text { at } W T 12,+5.25 \mathrm{~V} \pm 0.25 \mathrm{~V} .
\end{gathered}
$$

Adjust V -R5 if necessary to correct the $+20-\mathrm{V}$ terminal voltage.
d. Set the power-line voltage to 100 V rms. Repeat step c; record the measurements.
e. Reset the line to 125 V rms. Measure and record the dc voltages as in steps c and d . Reset the line to 115 V rms.
f. Verify that none of the 3 dc voltages varies more than $3 \%$ (total) between steps $d$ and e. Otherwise, one or more of the regulators has failed.

Detailed trouble analysis will not be described. Data in Table 5-2 may be helpful. No-load transformer voltages are about $5 \%$ higher than the tabulated (operating) values. The voltage drops across series resistors V-R3, V-R9, and V-R10 will serve to measure corresponding currents, and thereby estimate the terminal currents of the power supply.

Table 5-2
POWER-SUPPLY PARAMETERS

| Circuit | Terminals (V-) | Parameter | Tolerance |
| :---: | :--- | :---: | :---: |
|  |  |  |  |
| Transformer |  |  |  |
|  | WT1-WT2 | 20.8 V ac | $\pm 15 \%$ |
| WT3-WT2 | 20.8 V ac | 15 |  |
| +20-V | WT8-WT9 | 8.4 V ac | 15 |
| $-20-\mathrm{V}$ | WT6 | 93 mA dc | 10 |
| $+5.25-\mathrm{V}$ | WT7 | 86 mA dc | 10 |
|  | WT12 | 330 mA dc | 10 |



Figure 5-3. Interior bottom view.

Removal of the load from any power-supply circuit simply requires unsoldering of the corresponding wires.

If the power-supply board is replaced, repeat steps a through f .

### 5.5.2 Definition of Problem Input.

If possible determine the nature of the problem-input signal from the original complaint, such as a report of failure to pass paragraph 5.2.4 of the minimum performance standards. Unless the failure is catastrophic, it may depend on frequency and amplitude of the input signal. If
such information is available, skip to step f; if unavailable, proceed as follows:
a. Use the appropriate signal generator (listed in Table $5-1$ ). Set the modulation selector to CW, frequency to 500 MHz , and level to -7 dBm ( 100 mV at the scaler INPUT). Set the scaler controls clockwise (to standard settings).
b. Connect the counter to the SYNC OUT jack and determine whether it reads properly ( 5 MHz ).
c. If there is no malfunction, tune to other frequencies until incorrect scaling is demonstrated. Investigate at least 1 frequency per octave, down to 1 MHz .
d. If necessary: raise the carrier level 4 dB , reset the SENSITIVITY control appropriately, and repeat step c.
e. Repeat step d until incorrect scaling is demonstrated. If necessary, cover the range $0.1-3 \mathrm{~V}$ in 7 steps of about 4 dB each.
f. Verify that the "problem-input" signal (one which results in faulty scaling) is within the specified ranges of frequency and level: $1-500 \mathrm{MHz}, 0.1-7 \mathrm{~V}$ rms.

### 5.5.3 Input Circuitry. Figures 6-3, 6-6.

The following procedure checks the attenuator and meter and also establishes a test signal for later checks.
a. Provide the problem-input signal of paragraph 5.5.2 at the INPUT connector.
b. Turn the SENSITIVITY control until the meter reads in the green shaded area.
c. If this is impossible, make a detailed trouble analysis of the pertinent connectors, wiring, attenuator, and meter circuitry.
d. Check the meter, and adjust if necessary, as follows: Apply a $100-\mathrm{MHz}, 100-\mathrm{mV}$ signal as in paragraph 5.5.2, a. Adjust B-R5 to set pointer of INPUT LEVEL meter to left edge of green sector.
e. If the meter responds normally, proceed to the next paragraph.

### 5.5.4 Input Amplifier, B Board.

The following procedure applies to the input amplifier and completes the checkout from INPUT connector through the B board.
a. Disconnect the jumper cable from B-J2. Connect the output at B-J2 to the sampling scope. Use the adaptor and blocking capacitor listed in Table 5-1 (874-QMDP and 874-K).
b. Verify that the displayed waveform is satisfactory by comparison with Figure 5-4.
c. If the criteria of step b are met, replace the cable (step a) and proceed to the next paragraph.
d. If the criteria of step $b$ are not met, return the $B$ board to General Radio Company for repair or replacement.
e. If a replacement B-board is installed, check the meter adjustment, described in paragraph 5.5.3. Check the instrument by the method of paragraph 5.2.

### 5.5.5 First Divider, C Board. Figure 6-7.

The following procedure applies to the trigger generator and binary divider and completes the checkout from the INPUT connector through the $C$ board.
a. Disconnect the jumper cable from C-J2. Connect the output from C-J2 to the sampling scope.
b. Verify that the displayed waveform is satisfactory by comparison with Figure 5-4 and the following comments. The period of the pulse should be exactly twice that of the INPUT signal. Examine the waveform carefully for irregu-
larities such as skipping, pairing, or grouping of pulses. If these are found, check the observation, if possible, by changing the INPUT signal to one that the scaler handles properly. (The irregularity should disappear).
c. If the waveform of step $b$ is satisfactory, replace jumper cable and proceed to next paragraph.
d. If the waveform of step $b$ is unsatisfactory, the C-board is probably at fault. Return it to General Radio Company for repair or replacement.
e. After installing a replacement C-board, check its performance as in step b. If necessary make the following adjustments; use a $500-\mathrm{MHz}, 100-\mathrm{mV}$ signal as before, and set the SENSITIVITY control fully cw :
(1) Monitor dc voltage at $\mathrm{C}-\mathrm{J} 3$ with electronic voltmeter; SYNC OUT signal with counter.
(2) Adjust C-R19 for 15.5 V dc at $\mathrm{C}-\mathrm{J} 3$.
(3) Adjust C-R9 to center of a range of settings that give proper counter readout ( 5 MHz ). If no such range can be found, try other settings of C-R19, such as $15,16,14,17$ V; adjust C-R9.
(4) Turn C-R19 over its range of settings that give proper counter readout, and note the corresponding voltage range measured at C-J3.
(5) Change the input signal from 500 MHz to 1 MHz , and repeat step (4).
(6) The ranges noted in steps (4) and (5) should overlap. Adjust C-R19 to the center of the overlapping voltage range.
(7) Return the frequency to 500 MHz and trim C-R9 if necessary as in step (3).

### 5.5.6 First Decade, C and D Boards. Figures 6-7, 6-11.

The following procedure applies to the by-5 divider and completes the checkout from the INPUT connector through the divide-by-ten circuitry and the 10/100 OUT connector.
a. Connect the counter to the 10/100 OUT connector and switch the MULTIPLY . . BY control to 10.

## NOTE

If the problem-input frequency is above 300 MHz , it will be necessary to use a second scaler, following the one being evaluated, to avoid exceeding the $30-\mathrm{MHz}$ input-frequency limit of the 1192 Counter.
b. Verify that the counter reads $1 / 10$ the input frequency (or $1 / 100$ the input frequency if two scalers are cascaded).
c. Disconnect the counter and connect the main output of scaler to the sampling scope instead. Compare the displayed amplitude and waveform with Figure 5-4.
d. Verify that the output meets these specifications: rectangular waveshape, amplitude greater than +0.5 Vpk ., duty ratio more than $50 \%$.


Figure 5-4. Typical waveforms at interior and panel-mounted connectors. All vertical scales are approximately $200 \mathrm{mV} / \mathrm{div}$, and represent voltage across a $50-\Omega$ load (the scope input impedance). These waveforms were photographed on a Tektronix 661 sampling oscilloscope with Type 4S1 ( 350 ps ) and 5T1 plug-in units.
e. Check for loose connections by applying small forces to interconnecting cables in the instrument. Verify that no erratic changes occur in the scope display.
f. If loose connections are found, repair them and repeat steps a through d.
g. If the output is unsatisfactory (steps b and d), return the D-board to General Radio Company for repair or replacement.
h. If a replacement D-board is installed, check its performance as in paragraphs 5.5.6 and 5.5.7. Adjust D-R1 for the center of its range for proper output frequency when a $500-\mathrm{MHz}$ signal is applied to the INPUT and the meter reads in the green sector.
i. Change the input signal from 500 MHz to 1 MHz and verify that the proper output frequency is obtained. If necessary reset D-R1 slightly, but within the range found in step h.
j. If the output is satisfactory, disconnect the scope and proceed to the next paragraph.

### 5.5.7 Final Decade, on D Board.

The following procedure applies to the final, divide-byten, portion of the D-board and completes the over-all checkout.
a. Connect the counter to the 10/100 OUT connector and switch the MULTIPLY . . . BY control to 100.
b. Verify that the counter reads $1 / 100$ the input frequency.
c. Replace the counter with the sampling scope to look at the main output of scaler. Compare the displayed amplitude and waveform with Figure 5-4.
d. Verify that the output meets these specifications: rectangular waveshape, amplitude greater than +0.5 V pk ., duty ratio less than 50\%.
e. Check for loose connections by applying small forces to interconnecting cables in the instrument. Verify that no erratic changes occur in the scope display.
f. If loose connections are found, repair them and repeat steps a through d.
g. If the output is unsatisfactory (steps b and d), return the D-board to General Radio Company for repair or replacement.
$h$. If the output is satisfactory, no further service is required.

# Parts Lists and Diagrams-Section 6 

NOTE
Parts lists and etched-board drawings appear just before corresponding reference views or schematic diagrams.
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## NOTE

Each reference designator used in our schematic diagrams and circuit descriptions now includes an initial letter, before a hyphen, to identify the subassembly. The numeric portion of each designator is generally shorter than would be the case if a block of numbers were assigned to each subassembly. A new designation WT (wiretie point) replaces the customary AT (anchor terminal). The letter before the hyphen may be omitted only if clearly understood, as within a subassembly schematic diagram.

Examples: B-R8 = B board, re:stor 8; D-WT2 = $D$ board, wire-tie point 2; CR6 oil the $V$ schematic is a shortened $f 0 \cdot m$ of $\because-C R 6=V$ board, diode 6. The instrument may consain A-R1, B-R1, C-R1, and D-R1

|  |  | MECHANICAL PARTS LIST |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Qnt. | No. | Name | Description | GR Part Number | FMC | Mfg. Part No. | Stoc FSN |
| 1 | 1 | CABINET ASM. | Enclosure, including feet and bail. | 4181-2528 | 24655 | 4181-2528 |  |
| 1 | 2 | METER | Meter, INPUT LEVEL, A-M1. | 5730-1420 | 40931 | 20504010-017 |  |
| 2 | 3 | KNOB ASM. | Knob, SENSITIVITY; MULTIPLY-BY, including retainer 52205402. | 5500-5221 | 24655 | 5500-5221 |  |
| 1 | 4 | GASKET | Cabinet gasket. | 5331-3086 | 24655 | 5331-3086 |  |
| 1 | 5 | FOOT | Right-front rigid foot. | 5250-2121 | 24655 | 5250-2121 |  |
| 2 | 6 | JACK | Jack, A-J2, SYNC OUT; A-J3, 10/100 OUT. | 4230-2301 | 09408 | UG-1094A/U |  |
| 1 | 7 | CONNECTOR | Coaxial, A-J1, INPUT. | 0874-4624 | 24655 | 0874-4624 |  |
|  | 8 | FOOT | Left-front rigid foot. | 5250-2120 | 24655 | 5250-2120 |  |
|  | - | BAIL | Folding front leg. | 5250-2123 | 24655 | 5250-2123 |  |
| 1 | 9 | SWITCH | Slide switch, A-S4, line voltage. | 7910-0831 | 42190 | 4603 |  |
| 2 | 10 | FUSEHOLDER | Fuse-mounting device. | 5650-0100 | 71400 | HKP-H | 5920-284-7144 |
| 1 | 11 | COVER PLATE | Cover plate, INPUT. | 0480-8190 | 24655 | 0480-8190 |  |
| 2 | 12 | FOOT | Rear resilient foot. | 5260-2060 | 24655 | 5260-2060 |  |
| 1 | 13 | PLUG | Power plug, $\mathrm{A}-\mathrm{J} 4$. | 4240-0600 | 24655 | 4240-0600 | 5935-816-0254 |



Figure 6-1. Front view, mechanical replaceable parts identified.


Figure 6-2. Rear view, mechanical replaceable parts identified.

## FEDERAL MANUFACTURER'S CODE

From Federal Supply Code for Manufacturers Cataloging Handbooks H4-1
(Name to Code) and H4-2 (Code to Name) as supplemented through August, 1968.

| Code | Manufacturer | Code |
| :---: | :---: | :---: |
| 00192 | Jones Mfg. Co, Chicago, Illinois | 49671 |
| 00194 | Walsco Electronics Corp, L.A., Callf. | 49956 |
| 00434 | Schweber Electronics, Westburg, L.l., N.Y. | 53021 |
| 00656 | Aerovox Corp, New Bedford, Mass, | 54294 |
| 01009 | Alden Products Co, Brockton, Mass. | 54715 |
| 01121 | Allen-Bradley, Co, Mllwaukee, Wisc. | 56289 |
| 01295 | Texas Instruments, Inc, Dallas, Texas | 59730 |
| 02114 | Ferroxcube Corp, Saugertles, N.Y. 12477 | 59875 |
| 02606 | Fenwal Lab Inc, Morton Grove, III. | 60399 |
| 02660 | Amphenol Electron Corp, Broadview, III. | 61637 |
| 02768 | Fastex, Des Plaines, III. 60016 | 61864 |
| 03508 | G.E. Semicon Prod, Syracuse, N.Y. 13201 | 63060 |
| 03636 | Grayburne, Yonkers, N.Y. 10701 | 63743 |
| 03888 | Pyrofilm Resistor Co, Cedar Knolls, N.J. | 65083 |
| 03911 | Clalrex Corp, New York, N.Y. 10001 | 65092 |
| 04009 | Arrow-Hart \& Hegeman, Hartford, Conn. 06106 | $\begin{aligned} & 70485 \\ & 70563 \end{aligned}$ |
| 04713 | Motorola, Phoenlx, Ariz. 85008 | 70903 |
| 05170 | Engr'd Electronics, Santa Ana, Calif. 92702 | 71126 |
| 05624 | Barber-Colman Co, Rockford, III. 61101 | 71294 |
| 05820 | Wakefield Eng, Inc, Wakefield, Mass. 01880 | 71400 |
| 07126 | Digitron Co, Pasadens, Callf. | 71468 |
| 07127 | Eagle Signal (E.W. Bliss Co), Baraboo, Wisc. | 71590 |
| 07261 | Avnet Corp, Culver City, Calif. 90230 | 71666 |
| 07263 | Fairchlld Camera, Mountain View, Callf. | 71707 |
| 07387 | Birtcher Corp, No. Los Angeles, Callf. | 71744 |
| 07595 | Amer Semicond, Arlington Hts, III. 60004 | 71785 |
| 07828 | Bodine Corp, Bridgeport, Conn. 06605 | 71823 |
| 07829 | Bodine Electric Co, Chicago, III. 60618 | 72136 |
| 07910 | Cont Device Corp, Hawthorne, Callf. | 72259 |
| 07983 | State Labs Inc, N.Y., N.Y. 10003 | 72619 |
| 07999 | Borg Inst., Delavan, Wisc. 53115 | 72699 |
| 08730 | Vemaline Prod Co, Franklin Lakes, N.J. | 72765 |
| 09213 | G.E. Semiconductor, Buffalo, N.Y. | 72825 |
| 09408 | Star-Tronics Inc, Georgetown, Mass, 01830 | 72962 |
| 09823 | Burgess Battery Co, Freeport, III. | 72982 |
| 09922 | Burndy Corp, Norwalk, Conn. 06852 | 73138 |
| 11236 | C.T.S. of Berne, Inc, Berne, Ind. 46711 | 73445 |
| 11599 | Chandler Evans Corp, W. Hartford, Conn. | 73559 |
| 12040 | Natlonal Semiconductor, Danbury, Conn. | 73690 |
| 12498 | Crystalonics, Cambridge, Mass. 02140 | 73899 |
| 12672 | RCA, Woodbridge, N.J. | 74193 |
| 12697 | Clarostat Mfg Co, Inc, Dover, N.H. 03820 | 74861 |
| 12954 | Dickson Electronics, Scottsdale, Ariz. | 74970 |
| 13327 | Solitron Devices, Tappan, N.Y. 10983 | 75042 |
| 14433 | ITT Semicondictors, W.Palm Beach, Fla. | 75382 |
| 14655 | Cornell-Dubilier Electric Co, Newark, N.J. | 75491 |
| 14674 | Corning Glass Works, Corning, N.Y. | 75608 |
| 14936 | General Instrument Corp, Hicksville, N.Y. | 75915 |
| 15238 | ITT, Semiconductor Div, Lawrence, Mass. | 76005 |
| 15605 | Cutlet-Hammer Inc, Milwaukee, Wisc. 53233 | 76149 |
| 16037 | Spruce Pine Mica Co, Spruce Pine, N.C. | 76487 |
| 17771 | Singer Co, Diehl Div, Somerville, N.J. | 76545 |
| 19396 | Illinois Tool Works, Pakton Div, Chicago, Ili. | 76684 |
| 19644 | LRC Electronics, Horseheads, N.Y. | 76854 |
| 19701 | Electra Mfg Co, Independence, Kanses 67301 | 77147 |
| 21335 | Fafnir Bearing Co, New Briton, Conn. | 77166 |
| 22753 | UID Electronics Corp, Hollywood, Fia. | 77263 |
| 23342 | Avnet Electronics Corp, Franklin Park, Ill. | 77339 |
| 24446 | G.E., Schenectady, N.Y. 12305 | 77642 |
| 24454 | G.E., Electronics Comp, Syracuse, N.Y. | 77630 |
| 24455 | G.E. (Lamp Div), Nela Park, Cleveland, Ohio | 77638 |
| 24655 | General Radio Co, W. Concord, Mass. 01781 | 78189 |
| 26806 | American Zettlet Inc, Costa Mese, Callf. | 78277 |
| 28520 | Hayman Mfg Co, Kenilworth, N.J. | 78488 |
| 28959 | Hoffman Electronics Corp, El Monte, Calif. | 78553 |
| 30874 | I.B.M, Armonk, New York | 79089 |
| 32001 | Jensen Mfg. Co, Chlcago, III. 60638 | 79725 |
| 33173 | G.E. Comp, Owensboro, Ky. 42301 | 79963 |
| 35929 | Constanta Co, Mont. 19, Que. | 80030 |
| 37942 | P.R. Mallory \& Co Inc, Indianapolis, Ind. | 80048 |
| 38443 | Marlin-Rockwell Corp, Jamestown, N.Y. | 80131 |
| 40931 | Honeywell Inc, Minneapolis, Minn. 55408 | 80183 |
| 42190 | Muter Co, Chicago, III. 60638 | 80211 |
| 42498 | National Co, Inc, Melrose, Mass. 02176 | 80258 |
| 43991 | Norma-Hoffman, Stanford, Conn. 06904 | 80294 |

## Manufacturer

RCA New York, N. Y. 10020
Raytheon Mfg Co, Waltham, Mass. 02154 Raytheon Mfg Co, Waltham, Mass. 02154 Sangamo Elactric Co, Springfield, III. 62705 Shatlcross Mig Co, Selma, N.C. Shure Brothers, Inc, Evanston, III Sprague Electric Co, N. Adams, Mass. Thomas and Betts Co, Elizabeth, N.J. 07207 TRW Inc, (Accessories Div), Cleveland, Ohio Torrington Mfg Co, Torrington, Conn Union Carbide Corp, New York, N.Y. 1001 United-Carr Fastener Corp, Boston, Mass. Victoreen Instrument Co, Inc, Cleveland, $O$. Ward Leonard Electric Co, Mt. Vernon, N.Y Westinghouse (Lamp Div), Bloomfield, N.J.
Weston Instruments, Newark, N.J.
Atlantic-India Rubber, Chicago, III. 60607 Amperite Co, Union City, N.J. 07087 Beiden Mig Co, Chicago, Ill. 60644 Bronson, Homer D, Co, Beacon Falls, Conn. Canfield, H.O. Co, Clifton Forge, Va. 24422 Bussman (McGraw Edison), St. Louls, Mo. ITT Cannon Elec, L.A., Calif. 90031 Centralab, Inc, Mllwaukee, Wisc, 53212 Continental Carbon Co, Inc, New York, N. Y. Coto Coll Co Inc, Providence, R.I. Chicago Miniature Lamp Works, Chicago, 111 Cinch Mfg Co, Chicago, III. 60624 Darnell Corp, Ltd, Downey, Calif. 90241 Electro Motive Mfg Co, Wilmington, Conn Electro Motive Mfg Co, Wilmington, Conn.
Nytronics Inc, Berkeley Helghts, N.J. 07922 Nytronics Inc, Berkeley Heights, N.J.
Dialight Co, Brooklyn, N.Y. 11237 Dialight Co, Brooklyn, N.Y. 11237
General Instr Corp, Newark, N.J. 07104 Drake Mfg Co, Chicago, III. 60656 Hugh H. Eby inc, Philadelphla, Penn. 1914 Hugh H. Eby Inc, Philadelphla, Penn. 191 Erie Technological Products Inc, Erie, Penn. Erie Technological Products Inc, Erie,
Beckman Inc, Fullerton, Calif. $\mathbf{9 2 6 3 4}$ Beckman Inc, Fullerton, Calif. 92634
Amperex Electronics Co, Hicksville, N. Amperex Electronics Co, Hicksvilie, N. Carling Electric Co, W. Hartford, C
Elco Resistor Co, New York, N.Y. Elco Resistor Co, New York, N.Y. JFD Electronics Corp, Brooklyn, N.Y Helnemann Electric Co, Trenton, N.J Industrial Condenser Corp, Chicago, lii. E.F. Johnson Co, Waseca, Minn. 5609
IRC Inc, Philadelphis, Penn. 19108 IRC Inc, Philadelphia, Penn. 19108
Kulka Electric Corp, Mt. Vernon, N. Y Kulka Electric Corp, Mt. Vernon, N.Y.
Lafayette Industrial Electronics, Jemica, N.Y Linden and Co, Providence, R.I. Littelfuse, Inc, Des Plaines, III. 60016 Lord Mfg Co, Erle, Penn. 16512 Mallory Electric Corp, Detrolt, Mich. 48204 James Millen Mfg Co, Malden, Mass. 02148 Mueller Electric Co, Cleveland, Ohio 44114 National Tube Co, Pittsburg, Penn. Oak Mfg Co, Crystal Lake, III. Patton MacGuyer Co, Providence, R.I. Pass-Seymour, Syracuse, N.Y. Plerce Roberts Rubber Co, Trenton, N.J. Positive Lockwasher Co, Newark, N.J. Ray-O-Vac Co, Madison, Wisc. TRW, Electronic Comp, Camden, N.J. 08103 General Instruments Corp, Brooklyn, N.Y. Shakeproof (III. Tool Works), Elgin, II. 60120 Sigma Instruments Inc, S. Braintree, Mass. Stackpole Carbon Co, St. Marys, Penn. Tinnerman Products, Inc, Cleveland, Ohlo RCA, Rec Tube \& Semicond, Harrison, N.J. Wiremold Co, Hartford, Conn. 06110 Zierick Mfg Co, New Rochelie, N.Y. Zierick Mfg Co, New Rocheile, Fastener, Toledo, Ohlo Vrestole Fastener, Yoledo,
Electronic Industries Assoc, Washington, D.C. Electronic Industries Assoc, Washington, Motorola Inc, Franklin Park, III. 60131 Motorola Inc, Franklin Park, III.
Standard Oil Co, Lafeyette, Ind. Standard Oil Co, Lafeyette, Ind.
Bourns Inc, Rlverside, Calif. 92506

| Code | Manufacturer |
| :---: | :---: |
| 80431 | Air Fifter Corp, Mifwaukee, Wisc. 5321 |
| 80583 | Hammarlund Co, Inc, New York, N.Y. |
| 80740 | Beckman Instruments, Inc, Fullerton, Callf. |
| 81030 | International Insturment, Orange, Conn. |
| 81073 | Grayhill Inc, LaGrange, III. 60525 |
| 81143 | Isolantite Mfg Corp, Stirling, N.J. 07980 |
| 81349 | Military Specifications |
| 81350 | Joint Army-Navy Specifications |
| 81751 | Columbus Electronics Corp, Yonkers, N.Y. |
| 81831 | Filtron Co, Flushing, L.I., N.Y. 11354 |
| 81840 | Ledex Inc, Dayton, Ohio 45402 |
| 81860 | Barry-Wright Corp, Watertown, Mass. |
| 82219 | Sylvania Elec Prod, Emporium, Penn. |
| 82273 | Indiana Pattern \& Model Works, LaPort, Ind. |
| 82389 | Switcheraft Inc, Chicago, III. 60630 |
| 82647 | Metais \& Controls Inc, Attleboro, Mass. |
| 82807 | Milwaukee Resistor Co, Milwaukee, Wisc. |
| 83033 | Meissner Mfg, (Maguire Ind) Mt. Carmel, III. |
| 83058 | Carr Fastener Co, Cambridge, Mass. |
| 83186 | Victory Engineering, Springfield, N.J. 07081 |
| 83361 | Bearing Speciaity Co, San Francisco, Callf. |
| 83587 | Solar Electric Corp, Warren, Penn. |
| 83740 | Union Carbide Corp, New York, N.Y. 10017 |
| 83781 | National Electronics Inc, Geneva, III. |
| 84411 | TRW Capacitor Div, Ogallala, Nebr. |
| 84835 | Lehigh Metal Prods, Cambridge, Mass. 02140 |
| 84971 | TA Mfg Corp, Los Angeles, Calif. |
| 86577 | Precision Metal Prods, Stoneham, Mass. 02180 |
| 86684 | RCA (Elect. Comp \& Dev), Harrison, N.J. |
| 86687 | REC Corp, New Rochelle, N.Y. 10801 |
| 86800 | Cont Electronics Corp, Brooklyn, N.Y. 11222 |
| 88140 | Cutler-Hammer Inc, Lincoln, III. |
| 88219 | Gould Nat. Batteries Inc, Trenton, N.J. |
| 88419 | Cornell-Dubilier, Fuquay-Varina, N.C. |
| 88627 | K \& G Mfg Co, New York, N.Y. |
| 89482 | Holtzer-Cabot Corp, Boston, Mass. |
| 89665 | United Triansformer Co, Chicago, Ill. |
| 90201 | Maltory Capacitor Co, Indianapolis, Ind. |
| 90750 | Westinghouse Electric Corp, Boston, Mass. |
| 90952 | Hardware Products Co, Reading, Penn, 19602 |
| 91032 | Continental Wire Corp, York, Penn. 17405 |
| 91146 | ITT (Cannon Electric Inc), Salem, Mass. |
| 91293 | Johanson Mfg Co, Boonton, N.J. 07005 |
| 91506 | Augat Inc, Attleboro, Mass. 02703 |
| 91598 | Chandler Co, Wethersfield, Conn. 06109 |
| 91637 | Dale Electronics Inc, Columbus, Nebr. |
| 91662 | Elco Corp, Willow Grove, Penn. |
| 91719 | General Instruments, Inc, Dallas, Texas |
| 91929 | Honeywell inc, Freeport, III. |
| 92519 | Electra Insul Corp, Woodside, L.l., N.Y. |
| 92678 | E.G.\&G., Boston, Mass, |
| 93332 | Sylvania Elect Prods, Inc, Woburn, Mass. |
| 93916 | Cramer Products Co, New York, N.Y. 10013 |
| 94144 | Raytheon Co, Components Div, Quincy, Mass. |
| 94154 | Tung Sol Electric Inc, Newerk, N.J. |
| 95076 | Garde Mfg Co, Cumberland, R.I. |
| 95121 | Quallty Components Inc, St. Mary's, Penn. |
| 95146 | Alco Electronics Mfg Co, Lawrence, Mass. |
| 95238 | Continental Connector Corp, Woodside, N.Y. |
| 95275 | Vitramon, Inc, Bridgeport, Conn. |
| 95354 | Methode Mfg Co, Chicago, III. |
| 95412 | General Electric Co, Schenectady, N.Y. |
| 95794 | Anaconda Amer Brass Co, Torrington, Conn. |
| 96095 | Hi-Q Div. of Aerovox Corp, Orlean, N.Y. |
| 96214 | Texas Instruments Inc, Dallas, Texas 75209 |
| 96256 | Thordarson-Meissner, Mt. Carmel, III. |
| 96341 | Microwave Associates Inc, Burlington, Mass. |
| 96791 | Amphenol Corp, Jonesville, Wisc, 53545 |
| 96906 | Military Standards |
| 98291 | Sealectro Corp, Mamaroneck, N. Y. 10544 |
| 98474 | Compar Inc, Buriingame, Calif. |
| 98821 | North Hills Electronics Inc, Glen Cove, N.Y. |
| 99180 | Transitron Electronics Corp, Melrose, Mass. |
| 99313 | Varian, Palo Alto, Callif. 94303 |
| 99378 | Atlee Corp, Winchester, Mass. 01890 |
| 99800 | Delevan Electronics Corp, E. Aurora, N.Y. |


| RESISTANCE IS IN OHMS, $K=10^{3}, \mathrm{M}=10^{6}$ <br> CAPACITANCE IS IN FARADS, $\mu=10^{-6}, p=10^{-12}$ <br> VOLTAGES EXPLAINED IN INSTRUCTION BOOK SERUCE NOTES $O$ =SCREWPNEL CONTROL WT.....REAR CONTROL COMPEETE REFRENEEEDESIGNATION INCLUDES SUBASSEMBL LETTER,C-R1,-R-RI, ETC. |  |  |
| :---: | :---: | :---: |

front

s3
rear

s2
front

section




## ELECTRICAL PARTS LIST

| Ref. Desig | g. Description | GR Part No. | FMC | Mfg. Part No. | Fed. Stock No. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| CAPACITORS |  |  |  |  |  |
| A-C1 | Electrolytic, $300 \mu \mathrm{~F}+100-10 \% 75 \mathrm{~V}$ | 4450-5620 | 37942 | 20-222544990 | 5910-931-7040 |
| A-C2 | Electrolytic, $1600 \mu \mathrm{~F}+100-10 \% 10 \mathrm{~V}$ | 4450-5603 | 37942 | 20-22406990 | 5910-931-7042 |
| FUSES |  |  |  |  |  |
| A-F1 | 2/10A, Slo-blo | 5330-0600 | 71400 | MDL, . 2 Amp . |  |
| A-F2 | 1/10A, Slo-blo | 5330-0400 | 71400 | MDL, . 1 Amp. | 5920-356-2185 |
| JACKS |  |  |  |  |  |
| A-J1 | INPUT | 0874-4624 | 24655 | 0874-4624 |  |
| A-J2 | 100:1 SYNC OUT | 4230-2301 | 09408 | UG-1094A/U |  |
| A-J3 | 10:1/100:1 OUT | 4230-2301 | 09408 | UG-1094A/U |  |
| A-J4 | Power plug | 4240-0600 | 24655 | 4240-0600 | 5935-816-0254 |
| METER |  |  |  |  |  |
| A-M1 | INPUT LEVEL | 5730-1420 | 40931 | 20504010-017 |  |
| PILOT LAMP |  |  |  |  |  |
| A-DS1 | Incandescent | 5600-0300 | 24454 | \#328 | 6240-155-7857 |
| RESISTORS |  |  |  |  |  |
| A-R1 | Film $150 \Omega \pm 1 \% 1 / 8 \mathrm{~W}$ | 6250-0150 | 75042 | CEA, $150 \Omega \pm 1 \%$ |  |
| A-R2 | Film $37.4 \mathrm{~K} \Omega \pm 1 \% 1 / 8 \mathrm{~W}$ | 6250-9374 | 75042 | CEA, $37.4 \mathrm{~K} \Omega \pm 1 \%$ |  |
| A-R3 | Film $150 \Omega \pm 1 \% 1 / 8 \mathrm{~W}$ | 6250-0150 | 75042 | CEA, $150 \Omega \pm 1 \%$ |  |
| A-R4 | Film $75 \Omega \pm 1 \% 1 / 8 \mathrm{~W}$ | 6250-0075 | 75042 | CEA, $75 \Omega \pm 1 \%$ |  |
| A-R5 | Film $121 \Omega \pm 1 \% 1 / 8 \mathrm{~W}$ | 6250-0121 | 75042 | CEA, $121 \Omega \pm 1 \%$ |  |
| A-R6 | Film $75 \Omega \pm 1 \% 1 / 8 \mathrm{~W}$ | 6250-0075 | 75042 | CEA, $75 \Omega \pm 1 \%$ |  |
| A-R7 | Film $61.2 \Omega \pm 0.5 \% 1 / 2 \mathrm{~W}$ | 6450-9612 | 75042 | CEA, $61.2 \Omega \pm 0.5 \%$ |  |
| A-R8 | Film $249 \Omega \pm 1 \% 1 / 8 \mathrm{~W}$ | 6250-0249 | 75042 | CEA, $249 \Omega \pm 1 \%$ |  |
| A-R9 | Film $61.9 \Omega \pm 1 \% 1 / 2 \mathrm{~W}$ | 6450-9619 | 75042 | CEC, $61.9 \Omega \pm 1 \%$ |  |
| A-R10 | Comp. $20 \mathrm{~K} \Omega \pm 5 \% 1 / 2 \mathrm{~W}$ | 6100-3205 | 01121 | RC20GF203J | 5905-192-0649 |
| SWITCHES |  |  |  |  |  |
| A-S1 | OFF | Part of A-S2 | --- | --- |  |
| A-S2 | MULTIPLY -- BY | 7890-5318 | 24655 | 7890-5318 |  |
| A-S3 | SENSITIVITY | 7890-5317 | 24655 | 7890-5317 |  |
| A-S4 | Line Voltage | 7910-0831 | 42190 | 4603 |  |
| TRANSFORMER |  |  |  |  |  |
| A-T1 | Power | 0745-4640 | 24655 | 0745-4640 |  |


| Ref. Desig. | Description | GR Part No. | FMC | Mfg. Part No. | Fed. Stock No. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| COMPLETE BOARD |  |  |  |  |  |
| B | Input-Amplifier Board, Dipped | 1157-4760 | 24655 | 1157-4760 |  |
| CAPACITORS |  |  |  |  |  |
| B-C1 | Ceramic, $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-1141 |
| B-C2 | Ceramic . $001 \mu \mathrm{~F}+80-20 \% 500 \mathrm{~V}$ | 4404-2109 | 72982 | $831, .001 \mu \mathrm{~F}+80-20 \%$ | 5910-938-9994 |
| B-C3 | Ceramic . $01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-1141 |
| B-C4 | Ceramic 10pF $\pm 10 \% 500 \mathrm{~V}$ | 4404-0108 | 72982 | $831,10 \mathrm{pF} \pm 10 \%$ |  |
| B-C5 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-1141 |
| B-C6 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-1141 |
| B-C7 | Ceramic 8.2pF (N30) $\pm 5 \% 500 \mathrm{~V}$ | 4411-9825 | 72982 | 0831003B1G00829J |  |
| B-C8 | Ceramic . $01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-1141 |
| B-C9 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, $.01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-1141 |
| B-C10 | Ceramic 7.5pF (30) $\pm 5 \% 500 \mathrm{~V}$ | 4411-9755 | 72982 | $831,7.5 \mathrm{pF}$ (30) |  |
| B-C11 | Ceramic $15 \mathrm{pF} \pm 10 \% 500 \mathrm{~V}$ | 4404-0158 | 72982 | $831,15 \mathrm{pF} \pm 10 \%$ |  |
| B-C12 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-1141 |
| B-C13 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-1141 |
| B-C14 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-1141 |
| B-C15 | Ceramic $.0022 \mu \mathrm{~F}+80-20 \% 500 \mathrm{~V}$ | 4404-2229 | 72982 | $831, .0022 \mu \mathrm{~F}+80-20 \%$ |  |
| B-C16 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-1141 |
| DIODES |  |  |  |  |  |
| B-CR1 | Type HD5000 | 6082-1021 | 73293 | HD5000 |  |
| B-CR2 | Type HD5000 | 6082-1021 | 73293 | HD5000 |  |
| B-CR3 | Type IN3604 | 6082-1011 | 24446 | IN3604 | 5961-995-2199 |
| INDUCTORS |  |  |  |  |  |
| B-L1 | Air-core | 1157-8301 | 24655 | 1157-8301 |  |
| B-L2 | Air-core | 1157-8300 | 24655 | 1157-8300 |  |
| INTEGRATED CIRCUIT |  |  |  |  |  |
| B-ICI | Linear | 5432-1439 | 04713 | MC1439G |  |
| JACKS |  |  |  |  |  |
| B-J1 | Connector | 4260-1800 | 15116 | 131-0141-0001 |  |
| B-J2 | Connector | 4260-1800 | 15116 | 131-0141-0001 |  |
| RESISTORS |  |  |  |  |  |
| B-R1 | Comp. $51 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0515 | 75042 | BTS, $51 \Omega \pm 5 \%$ |  |
| B-R2 | Comp. $330 \Omega \pm 10 \% 1 / 4 \mathrm{~W}$ | 6099-1339 | 75042 | BTS, $330 \Omega \pm 10 \%$ |  |
| B-R3 | Comp. $200 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-4205 | 75042 | BTS, $200 \mathrm{~K} \Omega \pm 5 \%$ | 5905-681-8821 |
| B-R4 | Comp. $200 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-4205 | 75042 | BTS, $200 \mathrm{~K} \Omega \pm 5 \%$ | 5905-681-8821 |
| B-R5 | Pot. Comp. $100 \mathrm{~K} \Omega \pm 20 \%$ | 6040-1000 | 01121 | FWC, $100 \mathrm{~K} \Omega 20 \%$ | 5905-958-7949 |
| B-R6 | Comp. $10 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0105 | 75042 | BTS, $10 \Omega 5 \%$ | 5905-809-8596 |
| B-R7 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| B-R8 | Comp. $2.7 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2275 | 75042 | BTS, $2.7 \mathrm{~K} \Omega 5 \%$ |  |
| B-R9 | Comp. $2 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2205 | 75042 | BTS, $2 \mathrm{~K} \Omega 5 \%$ | 5905-279-4629 |
| B-R10 | Comp. $82 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0825 | 75042 | BTS, $82 \Omega 5 \%$ |  |
| B-R11 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| B-R12 | Comp. $3 \mathrm{~K} \Omega \pm 5 \% 1 / 2 \mathrm{~W}$ | 6100-2305 | 01121 | RC20GF302J | 5905-279-1751 |
| B-R13 | Comp. 1.1 K $\Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2115 | 75042 | BTS, 1.1 K $\Omega 5 \%$ |  |
| B-R14 | Comp. $82 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0825 | 75042 | BTS, $82 \Omega 5 \%$ |  |
| B-R15 | Comp. $10 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0105 | 75042 | BTS, $10 \Omega 5 \%$ | 5905-809-8596 |
| B-R16 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| B-R17 | Comp. $1 \mathrm{~K} \Omega \pm 5 \% \mathrm{l} / 2 \mathrm{~W}$ | 6100-2105 | 01121 | RC20GF102J | 5905-195-6806 |
| B-R18 | Comp. $1 \mathrm{~K} \Omega \pm 5 \% 1 / 2 \mathrm{~W}$ | 6100-2105 | 01121 | RC20GF102J | 5905-195-6806 |
| B-R19 | Comp. $39 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0395 | 75042 | BTS, $39 \Omega 5 \%$ |  |
| B-R20 | Comp. $330 \Omega \pm 5 \% 1 / 2 \mathrm{~W}$ | 6100-1335 | 01121 | RC20GF331J | 5905-192-3971 |
| B-R21 | Comp. 1.6 K $\Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2165 | 75042 | BTS, $1.6 \mathrm{~K} \Omega 5 \%$ |  |
| B-R22 | Comp. $2 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2205 | 75042 | BTS, $2 \mathrm{~K} \Omega 5 \%$ | 5905-279-4629 |
| B-R23 | Comp. $15 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-3155 | 75042 | BTS, $15 \mathrm{~K} \Omega 5 \%$ | 5905-681-8818 |
| B-R24 | Comp. 1.6 K $\Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2165 | 75042 | BTS, $1.6 \mathrm{~K} \Omega 5 \%$ |  |
| B-R25 | Comp. $390 \Omega \pm 10 \% 1 / 4 \mathrm{~W}$ | 6099-1399 | 75042 | BTS, $390 \Omega 10 \%$ |  |
| B-R26 | Comp. $300 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1305 | 75042 | BTS, $300 \Omega 5 \%$ | 5905-279-5481 |
| B-R27 | Comp. $6.8 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2685 | 75042 | BTS, $6.8 \mathrm{~K} \Omega 5 \%$ | 5905-686-9997 |
| B-R28 | Comp. $2 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2205 | 75042 | BTS, $2 \mathrm{~K} \Omega 5 \%$ | 5905-279-4629 |
| SOCKETS |  |  |  |  |  |
| B-S01 | Transistor | 7540-3450 | 91506 | 8069-1G2 |  |
| B-S02 | Transistor | 7540-3450 | 91506 | 8069-1G2 |  |
| B-S03 | Transistor | 7540-3450 | 91506 | 8069-1G2 |  |
| TRANSISTORS |  |  |  |  |  |
| B-Q1 | Type 2N2857 | 8210-1088 | 24454 | 2N2810-A |  |
| B-Q2 T | Type 2N2857 | 8210-1088 | 24454 | 2N2810-A |  |
| B-Q3 | Type A485 | 8210-1194 | 73445 | A485 |  |


| Ref. Desig | ig. Description | GR Part No. | FMC | Mfg. Part No. | Fed. Stock No. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| COMPLETE BOARD |  |  |  |  |  |
| C | Binary-Frequency-Divider board Asm, Cpt. | 1157-4770 | 24655 | 1157-4770 |  |
| CAPACITORS |  |  |  |  |  |
| C-C1 | Ceramic 1000pF (GMV) 500 V | 4400-2094 | 01121 | SS5A |  |
| C-C2 | Ceramic . $01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| C-C3 | Ceramic $10 \mathrm{pF} \pm 10 \% 500 \mathrm{~V}$ | 4404-0108 | 72982 | 831, 10pF 10\% |  |
| C-C4 | Ceramic 1000pF (GMV) 500 V | 4400-2094 | 01121 | SS5A |  |
| C-C5 | Ceramic . $01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| C-C6 | Ceramic 1000pF (GMV) 500 V | 4400-2094 | 01121 | SS5A |  |
| C-C7* | Ceramic 4.7pF (N30) $\pm 5 \% 500 \mathrm{~V}$ | *4411-9475* | 72982 | 831, 4.7pF (N30)* |  |
| C-C8 | Ceramic 1000pF (GMV) 500 V | 4400-2094 | 01121 | SS5A |  |
| C-C9 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| C-C10 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| C-C11* | Ceramic $3.9 \mathrm{pF} \pm 5 \% 500 \mathrm{~V}$ | *4400-0600* | 78488 | GA, 3.9pF 5\%* |  |
| C-C12 | Ceramic . $01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| C-C13 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| C-C14 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, .01 $\mu \mathrm{F}+80-20 \%$ | 5910-974-5697 |
| C-C15 | Ceramic 10pF $\pm 10 \% 500 \mathrm{~V}$ | 4404-0108 | 72982 | $831,10 \mathrm{pF} 10 \%$ |  |
| C-C16 | Ceramic $0.1 \mu \mathrm{~F}+80-20 \% 10 \mathrm{~V}$ | 4431-4109 | 72982 | $5655,0.1 \mu \mathrm{~F}+80-20 \%$ |  |
| C-C17 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| C-C18 | Ceramic 20pF $\pm 10 \% 500 \mathrm{~V}$ | 4404-0208 | 72982 | $831,20 \mathrm{pF} 10 \%$ |  |
| C-C19 | Ceramic $0.1 \mu \mathrm{~F}+80-20 \% 10 \mathrm{~V}$ | 4431-4109 | 72982 | $5655,0.1 \mu \mathrm{~F}+80-20 \%$ |  |
| C-C20 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| C-C21 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, .01 $\mu \mathrm{F}+80-20 \%$ | 5910-974-5697 |
| C-C22 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| C-C23 | Ceramic 10pF $\pm 10 \% 500 \mathrm{~V}$ | 4404-0108 | 72892 | $831,10 \mathrm{pF} 10 \%$ |  |
| C-C24 | Ceramic $0.1 \mu \mathrm{~F}+80-20 \% 10 \mathrm{~V}$ | 4431-4109 | 72982 | $5655,0.1 \mu \mathrm{~F}+80-20 \%$ |  |
| C-C25 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| DIODES |  |  |  |  |  |
| C-CRI* | Tunnel Diode | 6085-1013* | 70754 | G05010C* |  |
| C-CR2* | Tunnel Diode | 6085-1012* | 70754 | G05005C* |  |
| C-CR3/CR | CR4* Matched Tunnel Diodes | 6085-1011* | 24655 | 6085-1011* |  |
| INDUCTORS |  |  |  |  |  |
| C-L1 | Air-core | 1157-8300 | 24655 | 1157-8300 |  |
| C-L2 | Air-core | 1157-8301 | 24655 | 1157-8301 |  |
| JACKS |  |  |  |  |  |
| C-J1 | Connector, | 4260-1800 | 15116 | 131-0141-0001 |  |
| C-J2 | Connector | 4260-1800 | 15116 | 131-0141-0001 |  |
| C-J3 | Connector | 4260-1291 | 70563 | 380598-1 |  |
| RESISTORS |  |  |  |  |  |
| C-R1 | Comp. $51 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0515 | 75042 | BTS, $51 \Omega 5 \%$ |  |
| C-R2 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| C-R3 | Comp. $2.2 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2225 | 75042 | BTS, $2.2 \mathrm{~K} \Omega 5 \%$ | 5905-723-5251 |
| C-R4 | Comp. 3.9 K $\Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2395 | 75042 | BTS, $3.9 \mathrm{~K} \Omega 5 \%$ |  |
| C-R5 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| C-R6 | Comp. $2.7 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2275 | 75042 | BTS, $2.7 \mathrm{~K} \Omega 5 \%$ |  |
| C-R7 | Comp. $110 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1115 | 75042 | BTS, $110 \Omega 5 \%$ |  |
| C-R8 | Comp. 3.6 K $\Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2365 | 75042 | BTS, $3.6 \mathrm{~K} \Omega 5 \%$ |  |
| C-R9 | Pot. Comp. $5 \mathrm{~K} \Omega \pm 20 \%$ | 6040-0600 | 01121 | FWC, $5 \mathrm{~K} \Omega 20 \%$ | 5905-034-5374 |
| C-R10 | Comp. 2.2 K $\Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2225 | 75042 | BTS, $2.2 \mathrm{~K} \Omega 5 \%$ | 5905-723-5251 |
| C-R11 | Comp. $150 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1155 | 75042 | BTS, $150 \Omega 5 \%$ | 5905-683-2243 |
| C-R12* | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | *6099-0335* | 75042 | BTS, $33 \Omega 5 \%$ * |  |
| C-R13* | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | *6099-0335* | 75042 | BTS, $33 \Omega 5 \% *$ |  |
| C-R14 | Comp. $2.7 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2275 | 75042 | BTS, $2.7 \mathrm{~K} \Omega 5 \%$ |  |
| C-R15 | Comp. $1 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2105 | 75042 | BTS, $1 \mathrm{~K} \Omega 5 \%$ | 5905-681-6462 |
| C-R16 | Comp. $3 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2305 | 75042 | BTS, $3 \mathrm{~K} \Omega 5 \%$ | 5905-682-4097 |
| C-R17 | Comp. 5.1 K $\Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2515 | 75042 | BTS, $5.1 \mathrm{~K} \Omega 5 \%$ | 5905-279-4623 |
| C-R18 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| C-R19 Pot | Pot. Comp. $500 \Omega \pm 20 \%$ | 6040-0300 | 01121 | FWC, 500 ${ }^{\text {20 }}$ 20\% | 5905-072-7795 |
| C-R21 | Comp. $470 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1475 | 75042 | BTS, $470 \Omega 5 \%$ | 5905-683-5242 |
| C-R22 | Comp. $510 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1515 | 75042 | BTS, $510 \Omega 5 \%$ | 5905-801-8272 |
| C-R23 | Comp. $51 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0515 | 75042 | BTS, $51 \Omega 5 \%$ |  |
| C-R24 | Film $64.9 \Omega \pm 1 \% 1 / 8 \mathrm{~W}$ | 6250-9649 | 75042 | CEA, $64.9 \Omega 1 \%$ |  |
| C-R25 F | Film $64.9 \Omega \pm 1 \% 1 / 8 \mathrm{~W}$ | 6250-9649 | 75042 | CEA, $64.9 \Omega 1 \%$ |  |
| C-R26 | Comp. $100 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1105 | 75042 | BTS, $100 \Omega 5 \%$ |  |
| C-R27 | Comp. $2.2 \mathrm{k} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2225 | 75042 | BTS, $2.2 \mathrm{~K} \Omega 5 \%$ | 5905-723-5251 |
| C-R28 | Comp. $100 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1105 | 75042 | BTS, $100 \Omega 5 \%$ |  |

* Parts listed above with asterisks are not recommended for replacement by the customer. They should be replaced only under GR factory control. If a set of spare parts is desired, please request the Binary-Frequency-Divider Board Assembly, Complete, P/N 1157-4770. This pretested subassembly includes all the C-prefix parts.

RESISTORS (Cont)

| C-R29 | Comp. $1 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2105 | 75042 | BTS, $1 \mathrm{~K} \Omega 5 \%$ | 5905-681-6462 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| C-R30 | Comp. $10 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0105 | 75042 | BTS, $10 \Omega 5 \%$ | 5905-809-8596 |
| C-R31 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| C-R32 | Comp. $2.7 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2275 | 75042 | BTS, $2.7 \mathrm{~K} \Omega 5 \%$ |  |
| C-R33 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| C-R34 | Comp. 1.3 K $\Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2135 | 75042 | BTS, $1.3 \mathrm{~K} \Omega 5 \%$ | 5905-686-3119 |
| C-R35 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| C-R36 | Comp. 3.3 K $\Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-2335 | 75042 | BTS, $3.3 \mathrm{~K} \Omega 5 \%$ | 5905-681-9969 |
| C-R37 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| C-R38 | Comp. $1 \mathrm{~K} \Omega \pm 5 \% 1 / 2 \mathrm{~W}$ | 6100-2105 | 01121 | RC20GF102J | 5905-195-6806 |
| C-R39 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| C-R40 | Comp. $100 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1105 | 75042 | BTS, $100 \Omega 5 \%$ |  |
| C-R41 | Comp. 1.3 K $\Omega \pm 5 \% 1 / 2 \mathrm{~W}$ | 6100-2135 | 01121 | RC20GF132J | 5905-279-1870 |
| SOCKETS |  |  |  |  |  |
| C-S04 | Transistor | 7540-3450 | 91506 | 8069-1G2 |  |
| C-S05 | Transistor | 7540-3450 | 91506 | 8069-1G2 |  |
| C-S06 | Transistor | 7540-3450 | 91506 | 8069-1G2 |  |
| TRANSISTORS |  |  |  |  |  |
| C-Q1* | Type 2N2857* | 8210-1088* | 24454 | 2N2810-A* |  |
| C-Q2* | Type 2N2857* | 8210-1088* | 24454 | 2N2810-A* |  |
| C-Q3* | Type 2N2857* | 8210-1088* | 24454 | 2N2810-A* |  |
| C-Q4 | Type 2N2857 | 8210-1088 | 24454 | 2N2810-A |  |
| C-Q5 | Type 2N2857 | 8210-1088 | 24454 | 2N2810-A |  |
| C-Q6 | Type A485 | 8210-1194 | 73445 | A485 |  |

* Parts listed above with asterisks are not recommended for replacement by the customer. They should be replaced only under GR factory control. If a set of spare parts is desired, please request the Binary-Frequency-Divider Board Assembly, Complete, P/N 1157-4770. This pretested subassembly includes all C-prefix parts.

| Ref. Desig. | Description | GR Part No. | FMC | Mfg. Part No. | Fed. Stock No. |
| :---: | :---: | :---: | :---: | :---: | :---: |
| COMPLETE BOARD |  |  |  |  |  |
| D-board | Divide-By-5 \& 10 Board, Cpt. | 1157-4780 | 24655 | 1157-4780 |  |
| CAPACITORS |  |  |  |  |  |
| D-Cl | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, $.01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| D-C2 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, . $01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| D-C3 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, $.01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| D-C4 | Ceramic $.01 \mu \mathrm{~F}+80-20 \% 100 \mathrm{~V}$ | 4401-3100 | 80131 | CC61, $.01 \mu \mathrm{~F}+80-20 \%$ | 5910-974-5697 |
| D-C6 | Electrolytic $4.7 \mu \mathrm{~F} \pm 20 \% 10 \mathrm{~V}$ | 4450-4700 | 56289 | 150D465X0015B2 | 5910-813-8160 |
| INTEGRATED CIRCUIT |  |  |  |  |  |
| D-ICl | Digital | 5431-9611 | 04713 | MC1013L |  |
| D-IC2 | Digital | 5431-9611 | 04713 | MC1013L |  |
| D-IC3 | Digital | 5431-9611 | 04713 | MC1013L |  |
| D-IC4 | Digital | 5431-9610 | 04713 | MC10131 |  |
| D-IC5 | Digital | 5431-9613 | 11293 | SF123-P |  |
| D-1C6 | Digital | 5431-8272 | 01295 | SN74H72N |  |
| JACKS |  |  |  |  |  |
| D-J1 | Connector | 4260-1800 | 15116 | 131-0141-0001 |  |
| D-J2 | Connector | 4260-1800 | 15116 | 131-0141-0001 |  |
| D-J3 | Connector | 4260-1800 | 15116 | 131-0141-0001 |  |
| D-J4 | Connector | 4260-1800 | 15116 | 131-0141-0001 |  |
| RESISTORS |  |  |  |  |  |
| D-R1 | Pot. Comp. $100 \Omega \pm 20 \%$ | 6040-0100 | 01121 | FWC, $100 \Omega 20 \%$ |  |
| D-R2 | Comp. $100 \Omega \pm 5 \%$ 1/8 W | 6098-1105 | 01121 | BB, $100 \Omega 5 \%$ |  |
| D-R3 | Comp. $51 \Omega \pm 5 \% 1 / 8 \mathrm{~W}$ | 6098-0515 | 01121 | BB, $51 \Omega 5 \%$ |  |
| D-R4 | Comp. $470 \Omega \pm 5 \% 1 / 8 \mathrm{~W}$ | 6098-1475 | 01121 | BB, $470 \Omega 5 \%$ |  |
| D-R5 | Comp. $470 \Omega \pm 5 \% 1 / 8 \mathrm{~W}$ | 6098-1475 | 01121 | BB, $470 \Omega 5 \%$ |  |
| D-R6 | Comp. $470 \Omega \pm 5 \% 1 / 8 \mathrm{~W}$ | 6098-1475 | 01121 | BB, $470 \Omega 5 \%$ |  |
| D-R7 | Comp. $470 \Omega \pm 5 \% 1 / 8 \mathrm{~W}$ | 6098-1475 | 01121 | BB, $470 \Omega 5 \%$ |  |
| D-R8 | Comp. $470 \Omega \pm 5 \% 1 / 8 \mathrm{~W}$ | 6098-1475 | 01121 | BB, $470 \Omega 5 \%$ |  |
| D-R9 | Comp. $39 \Omega \pm 5 \% 1 / 8 \mathrm{~W}$ | 6098-0395 | 01121 | BB, $39 \Omega 5 \%$ |  |
| D-R10 | Comp. $51 \Omega \pm 5 \% 1 / 8 \mathrm{~W}$ | 6098-0515 | 01121 | BB, $51 \Omega 5 \%$ |  |
| D-R11 | Comp. $470 \Omega \pm 5 \% 1 / 8 \mathrm{~W}$ | 6098-1475 | 01121 | BB, $470 \Omega 5 \%$ |  |
| D-R12 | Comp. $33 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0335 | 75042 | BTS, $33 \Omega 5 \%$ |  |
| D-R13 | Comp. $100 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1105 | 75042 | BTS, $100 \Omega 5 \%$ |  |
| D-R14 | Comp. $300 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1305 | 75042 | BTS, $300 \Omega 5 \%$ | 5905-279-5481 |
| D-R15 | Comp. $200 \Omega \pm 5 \%$ 1/4 W | 6099-1205 | 75042 | BTS, $200 \Omega 5 \%$ | 5905-892-0107 |
| D-R16 | Comp. $51 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0515 | 75042 | BTS, $51 \Omega 5 \%$ |  |
| D-R17 | Comp. $39 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0395 | 75042 | BTS, $39 \Omega 5 \%$ |  |
| D-R18 | Comp. $51 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-0515 | 75042 | BTS, $51 \Omega 5 \%$ |  |
| D-R19 | Comp. 200 ${ }^{\text {c }}$ (5\% 1/4 W | 6099-1205 | 75042 | BTS, $200 \Omega 5 \%$ | $5905-892-0107$ |
| D-R20 | Comp. $300 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$ | 6099-1305 | 75042 | BTS, $300 \Omega 5 \%$ | 5905-279-5481 |
| TRANSISTORS |  |  |  |  |  |
| D-Q1 | Type 2N4258 | 8210-1130 | 93916 | 2N4258 |  |
| D-Q2 | Type 2N4258 | 8210-1136 | 93916 | 2N4258 |  |
| D-Q3 | Type 2N4258 | 8210-1136 | 93916 | 2N4258 |  |
| D-Q4 | Type 2N4258 | 8210-1136 | 93916 | 2N4258 |  |
| D-Q5 | Type 2N4258 | 8210-1136 | 93936 | 2N4258 |  |
| D-Q6 | Type 2N4258 | 8210-1136 | 93916 | 2N4258 |  |

COMPLETE BOARD
V Power-Supply Board, Dipped

## CAPACITORS

| V-C1 | Electrolytic | $6.8 \mu \mathrm{~F} \pm 20 \%$ |
| :--- | :--- | :--- |
| V-C2 | Electrolytic | $15 \mu \mathrm{~F}$ |
| $\pm 20 \%$ | 20 V |  |

V-C3 Electrolytic $15 \mu \mathrm{~F} \pm 20 \% 20 \mathrm{~V}$
V-C4 Electrolytic $47 \mu \mathrm{~F} \pm 20 \% 6 \mathrm{~V}$

## DIODES

V-CR1 Type 1N3253
V-CR2 Type 1N3253
V-CR3 Type 1N3253
V-CR4 Type 1N3253
V-CR5 Type 1N3253
V-CR6 Type 1N3253
V-CR7 Type 1N3253
V-VR9 Type 1N753A $6.2 \mathrm{~V} \pm 5 \%$

## RESISTORS

V-R1 Comp. $10 \mathrm{~K} \Omega \pm 10 \% 1 / 4 \mathrm{~W}$ V-R2 Comp. $10 \mathrm{~K} \Omega \pm 10 \% 1 / 4 \mathrm{~W}$
V-R3 Comp. $2.7 \Omega \pm 5 \%$ l/4 W
V-R4 Comp. $13 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$
V-R5 Pot. Comp. $1 \mathrm{~K} \Omega \pm 20 \%$
V-R6 Comp. $6.2 \mathrm{~K} \Omega \pm 5 \% 1 / 4 \mathrm{~W}$
V-R7 Film $3.83 \mathrm{~K} \Omega \pm 1 \% 1 / 8 \mathrm{~W}$
V-R8 Film $4.02 \mathrm{~K} \Omega \pm 1 \% 1 / 8 \mathrm{~W}$
V-R9 Comp. $4.7 \Omega \pm 5 \% 1 / 4 \mathrm{~W}$
V-R10 Wire-wound $1.5 \Omega \pm 10 \% 2 \mathrm{~W}$
V-R11 Comp. $15 \mathrm{~K} \Omega \pm 10 \% 1 / 4 \mathrm{~W}$
V-R12 Film $1.78 \mathrm{~K} \Omega \pm 1 \% 1 / 8 \mathrm{~W}$
V-R13 Film $487 \Omega \pm 1 \% 1 / 8 \mathrm{~W}$
V-R14 Wire-wound $20 \Omega \pm 5 \% 2 \mathrm{~W}$
V-R15 Comp. 2.7 K $\Omega \pm 10 \% 1 / 4 \mathrm{~W}$

## TRANSISTORS

V-Q1 Type 40250V1
V-Q2 Type 2N3414
V-Q3 Type 2N3414
V-Q4 Type 2N3414
V-Q5 Type 2N3905
V-Q6 Type 2N3414
V-Q7 Type 2N3414
V-Q8 Type 40250 VI
V -Q9 Type 40250 V 1
V-Q10 Type 2N3414
V-Q11 Type 2N3414
V-Q12 Type 2N3414

1157-4750 24655 1157-4750

| $4450-5000$ | 56289 | 150D685X0035B |
| :--- | :--- | :--- |
| $4450-5200$ | 56289 | 150D156X0020B |
| $4450-5200$ | 56289 | 150D156X0020B |
| $4450-5500$ | 56289 | 150D476X0006B |


| $6081-1001$ | 79089 | 1N3253 | $5961-814-4251$ |
| :--- | :--- | :--- | :--- |
| $6081-1001$ | 79089 | 1N3253 | $5961-814-4251$ |
| $6081-1001$ | 79989 | 1N3253 | $5961-14-4251$ |
| $6081-1001$ | 79089 | 1N3253 | $5961-814-4251$ |
| $6081-1001$ | 79009 | 1N3253 | $5961-814-4251$ |
| $681-1001$ | 79089 | 1N3253 | $5961-14-4251$ |
| $6081-1001$ | 79089 | 1N3253 | $5961-814-4251$ |
| $6083-1006$ | 07910 | 1N753A | $5961-752-6121$ |


| 6099-3109 | 75042 | BTS, $10 \mathrm{~K} \Omega 10 \%$ |  |
| :---: | :---: | :---: | :---: |
| 6099-3109 | 75042 | BTS, $10 \mathrm{~K} \Omega \mathrm{l}$ |  |
| 6099-9275 | 75042 | BTS, $2.785 \%$ |  |
| 6099-3135 | 75042 | BTS, $13 \mathrm{~K} \Omega 5 \%$ | 5905-702-4439 |
| 6040-0400 | 01121 | FWC, $1 \mathrm{~K} \Omega 20 \%$ |  |
| 6099-2625 | 75042 | BTS, $6.2 \mathrm{~K} \Omega 5 \%$ | 5905-682-4100 |
| 6250-1383 | 75042 | CEA, $3.83 \mathrm{~K} \Omega 1 \%$ | 5905-827-3333 |
| 6250-1402 | 75042 | CEA, $4.04 \mathrm{~K} \Omega 1 \%$ | 5905-702-7231 |
| 6099-9475 | 75042 | BTS, $4.785 \%$ |  |
| 6760-9159 | 75042 | BWH, $1.5 \Omega 10 \%$ |  |
| 6099-3159 | 75042 | BTS, $15 \mathrm{~K} \Omega 10 \%$ |  |
| 6250-1178 | 75042 | CEA, $1.78 \mathrm{~K} \Omega 1 \%$ | 5905-824-3077 |
| 6250-0487 | 75042 | CEA, $487 \Omega 1 \%$ |  |
| 6760-0205 | 75042 | BWH, $20 \Omega 10 \%$ |  |
| 6099-2279 | 75042 | BTS, $2.7 \mathrm{~K} \Omega 10 \%$ |  |
| 8210-1158 | 12672 | 40250-V1 |  |
| 8210-1047 | 24446 | 2N3414 | 5961-989-2749 |
| 8210-1047 | 24446 | 2N3414 | 5961-989-2749 |
| 8210-1047 | 24446 | 2N3414 | 5961-989-2749 |
| 8210-1114 | 04713 | 2N3905 |  |
| 8210-1047 | 24446 | 2N3414 | 5961-989-2749 |
| 8210-1047 | 24446 | 2N3414 | 5961-989-2749 |
| 8210-1158 | 12672 | $40250-\mathrm{V} 1$ |  |
| 8210-1158 | 12672 | 40250-V1 |  |
| 8210-1047 | 24446 | 2N3414 | 5961-989-2749 |
| 8210-1047 | 24446 | 2N3414 | 5961-989-2749 |
| 8210-1047 | 24446 | 2N3414 | 5961-989-2749 |

NOTE
View shows component side of board. Circuit paths: solid=opposite side, shaded= this side.


Figure 6-4. B-assembly etched-circuit board (P/N 1157-4760).

NOTE
View shows component side of board. Circuit paths: this side not shown, shaded=opposite side.


Figure 6-5. C-assembly etched-circuit board ( $\mathrm{P} / \mathrm{N} 1157-4770$ ).

NOTE: The number etched on the foil is not the part number. The dot on the foil at the transistor socket indicates the collector lead.

| RESISTANCE IS IN OHMS，$K=10^{3}, M=10^{6}$ CAPACITANCE IS IN FARADS，$\mu=10^{-6}, p=10^{-12}$ <br> VOLTAGES EXPLAINED IN INSTRUCTION BOOK SERVICE NOTES $\square=P A N E L$ CONTROL ここここーこ＝REAR CONTROL <br> ＝SCREWDRIVER CONTROL WT＝WIRE TIE TP：TEST POINT COMPLETE REFERENCE DESIGNATION INCLUDES SUBASSEMBLY LETTER，C－RI，B－RI，ETC． |  | CONNECTIONS $\qquad$ OUTPUT LEAVES SUBASSEMBLY INPUT FROM DIFFERENT SUBASSEMBLY OUTPUT REMAINS ON SUBASSEMBLY INPUT FROM SAME SUBASSEMBLY |
| :---: | :---: | :---: |



Figure 6－6．Input Amplifier／Meter Drive diagram．B


[^2]

Figure 6-7. Trigger Generator/Binary Divider diagram.

NOTE
View shows component side of board. Circuit paths: shaded=this side, solid=opposite side. Component outlines: lined=this side, dashed=opposite side.


Figure 6-8. D-assembly etched-circuit board (P/N 1157-4780).


Figure 6-9. V-assembly etched-circuit board (P/N 1157-4750).

NOTE: The number etched on the foil is not the part number. The dot on the foil at the transistor socket indicates the collector lead.


WT14
$\mathrm{W}^{\circ} \mathrm{T} 13$

| RESISTANCE IS IN OHMS, $K=10^{3}, M=10^{6}$ <br> CAPACITANCE IS IN FARADS, $y=10^{-6}, p=10^{-12}$ <br> VOLTAGES EXPLAINED IN INSTRUCTION BOOK SERVICE NOTES $\square$ PANEL CONTROL $=こ=こ=$ REAR CONTROL <br> $\theta=S$ CREWDRIVER CONTROL WT = WIRE TIE TP =TEST POINT COMPLETE REFERENCE DESIGNATION INCLUDES SUBASSEMBLY LETTER, C-RI, B-RI, ETC. |  | CONNECTIONS $\qquad$ OUTPUT LEAVES SUbassembly input from different subassembly $\qquad$ output remains on subassembly input from same subassembly |
| :---: | :---: | :---: |



Figure 6-11. By-5 and By-10 Divider diagram. D

## DIFFERENCE DATA

## APPLICABLE TO EARLY PRODUCTION ONLY

For 1157-B Scaler Instruction Manual, Form 1157-0110 A, August 1969.

This difference data sheet adapts the manual to $1157-\mathrm{B}$ Scalers having ID number B100. The following changes do not apply to scalers made more recently.

## GENERAL.

Early production instruments of the lot No. ID-B100 have identical characteristics with later production, but differ in the circuitry for the last division by 5.

## SPECIFIC CHANGES.

Please make the indicated changes on the pages below. Bold-face type characterizes short additions (easily penciled in the manual) or reference notes to lengthy additions.

## page 4-4

Paragraph 4.3.6:
Delete the description starting with: Division by 5 takes place in D-IC5 and D-IC6 ... to the end of Paragraph 4.3.6.
Add this note: See difference data, page 6-10.

### 4.3.6 By-10 Divider-D

(First 2 paragraphs unchanged.) New 3rd. and last paragraph of 4.3.6:
To complete the division by 10 , the signal output from difference amplifier D-Q3/D-Q4 (from D-Q3 collector) drives the scale-of-5 divider IC5, at pin 1. The divided output from IC5, pin 8 , is $1 / 100$ the INPUT frequency, and has the $40 \%$ duty ratio characteristic of the main 100:1 OUTPUT. That signal emerges via difference amplifier D-Q5/D-Q6 and jack D-J3. The complementary signal from D-O5 collector) is connected via D-J4 to the SYNC OUT jack.
page 4-4
Figure 4-4:
Delete the curves labeled IC5A, IC5B, and Q/IC6.
Relabel the $\mathrm{Q} / \mathrm{IC} 6$ curve: IC5 pin 8.

Change the parts designated as follows:

| Reference <br> Desig. | Description | Part No. | FMC | Mfg. Part No. | Fed. Stock No. |
| :--- | :--- | :--- | :--- | :--- | :--- |
| D-IC5 | Digital Integrated circuit | $5431-9609$ | 42498 | SD 7262 |  |
| D-R19 | $130 \Omega 5 \% 1 / 4 \mathrm{~W}$ | $6099-1135$ | 75042 | BTS, $130 \Omega 5 \%$ | $5905-807-6269$ |
| D-R20 | $330 \Omega 5 \% 1 / 4 \mathrm{~W}$ | $6099-1335$ | 75042 | BTS, $330 \Omega 5 \%$ | $5905-686-3369$ |

page 6-9
Change Figure 6-11, the D-board schematic, as follows:

Connect R20 between Q6 base and ground (not to IC5). Substitute IC5 (new description) for both IC5 and IC6, with connections as follows: input from Q3 collector, pin I; output through R14 to Q5, pin 8; bias +5 V (bypassed to ground through C6), pin 5; ground points, pins 3, 6, and 10.

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*Repair services are available at these offices.

## GENERAL RADIO <br> WEST CONCORD, MASSACHUSETTS 01781


[^0]:    *For scalers with ID no. B100, refer to Difference Data in rear of manual.

[^1]:    * Equivalents may be substituted.

[^2]:    RESISTANCE IS IN OHMS, $K=10^{3}, M=10^{6}$
    CAPACITANCE IS IN
    CAPACITANCE IS IN FARADS, $\mu=10^{-6}, \quad$ P $=10^{-12}$
    VOLTAGES EXLAINED IN INSTRUTION BOK SERVICE NOTES $\square=P A N E L$ CONTROL $==-=-2$ REAR CONTROL $O=$ SCREWDRIVER CONTROL WT $=$ WIRE TIE TP TEST POINT
    COMPETE REFERENCE DESIGNATION INCLUDES SUBASSEMBLI COMPEETE REFERENCE
    LETTER,C-RI, B-RI, ETC.

